

# WIRE <br> iN <br> Electrical Construction. 

$\cdots$

JOHN A.ROEBLING'S SONS CO.

TRENTON, N. 3 .

California
egional
xcility


## WIRE

IN

## Electrical Construction

## John A. Roebling's Sons Co.

TRENTON, N. J.

117-119 Liberty street, New York.

32 South Water street, Cleveland.

171-173 Lake street, Chicago.

25-27 Fremont street, San Francisco.

を Be Brandt gores, trenton.

COPYRIGHTED, 1897,
BY
JOHN A. ROEBLING'S SONS CO.

All rights reserved.

$T K$
3305
$R 62 W$

## PREFATORY.

THE OBJECT of this book is to give in a convenient form the properties and dimensions of bare and insulated wires and cables used in electrical construction. No attempt has been made to describe the uses of wire in any of the applications of electricity. To go into this would require that the whole field of electrical engineering be covered.

It is believed that some of the matter is new. All of the tables have been very carefully computed, and are believed to be correct.

In nearly all cases the formulæ and constants used in computing tables are given, so that the user can determine at once the basis from which the table was calculated. A considerable amount of work has been done in testing samples to determine the proper constants. In many cases this has taken more time than the actual preparation of the tables.

It is hoped that the work will be acceptable to the users of electrical wires, and that some of the labor involved in the preparation of these tables will be saved to those using the book.

John A. Roebling's Sons Co.

Trenton, N. J., May, 1897.

## TABLE OF CONTENTS.

Mrasures and their Equivalents: ..... PAGE.
Measures of length ..... 1
Measures of area ..... 2
Measures of volume ..... 3
Measures of weight. ..... 4
Measures of work. ..... 5
Measures of pressure. ..... 6
Decimal equivalents of parts of an inch. ..... 7
Wire gauges in mils. ..... 8
Wire gauges in millimeters. ..... 9
Tables of specific gravities: ..... 10
Liquids ..... 11
Gases. ..... 11
Weights of substances. ..... 12
The comparison of thermometers:
Fahrenheit to Centigrade. ..... 13
Centigrade to Fahrenheit. ..... 13
Electrical units. ..... 14-15
COPPER WIRE:
Formulæ and explanations. ..... 16-17
Matthiessen's standard. ..... 17
Temperature coëfficients. ..... 18
Properties of copper wire-weights, resistances, etc.English system :
Brown \& Sharpe gauge. ..... 19
Birmingham wire gauge ..... 20
New British standard gauge. ..... 21
Metric system :
Brown \& Sharpe gauge. ..... 22
Weights of all gauges. ..... 23
Hard-drawn copper wire:
British Post-office specifications. ..... 24
Telephone specifications ..... 25
Tensile strength of copper wire. ..... 26
Bi-metallic wire. ..... 27
Strands of copper wire :
Formulæ and explanations. ..... 28
Diameters and properties. ..... 29
Diameters of wires in strands. ..... 30-31
Numbers of wires in strands. ..... 32-33
Iron Wire: page.
Formulæ and explanations. ..... 34
Properties of iron wire-weights, strength, resistances, etc., ..... 35
Specifications:
Western Union Telegraph company ..... 36
British Post-office. ..... 37
Strands:
Formulæ and explanations. ..... 38
Properties of galvanized steel wire strands-welghts and breaking strength. ..... 38
Supporting capacity of galvanized strands. ..... 39
Currents:
Fusing effects:
Diameters of wires. ..... 40
Current required. ..... 41
Heating effects:
References and explanations. ..... 42
Carrying capacity:
Insurance rules. ..... 43
Insulated wires in mouldings. ..... 44
Wires indoors. ..... 45
Wires outdoors. ..... 46
Spans:
Formulæ and explanations. ..... 47-49
Specifications. ..... 48
Strains at centers of spans. ..... 50-52
Total lengths of wires in spans. ..... 54-55
Deflections in spans at various temperatures. ..... 53
Description of the Roebling Electric Wires:
Weatherproof wires. ..... 56-57
Rubber wires. ..... 58-59
Magnet wire. ..... 60-61
German silver wire. ..... 62
Office wires. ..... 63
Cables:
Power cables. ..... 64-65
Telephone cables. ..... 66-67
Telegraph cables. ..... 68-69
Aerial cables. ..... 70-71
Submarine cables. ..... 72
Rall-bonds ..... 73
MEASURES OF LENGTH.

MEASURES OF AREA.

| Names of units. | Circular mils. | Square mils. | Square millimeters. | Square centimeters. | Square inches. | Square | Square yards. | Square meters. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Circular mils........... | 1. | . 7854 | . 0005067 |  |  | ............ | ............ | .......... |
| Square mils............ | 1.2732 | 1. | . 000645 | . 0000064 | . 000001 | ..... ...... | .......... | ........... |
| Square millimeters.. | 1973.5 | 1550.1 | 1. | .$^{.01}$ | . 00155 | .......... 001 | .......... | .......... |
| Square centimeters. | 197350. | 155010. | 100. | 1. |  | . 001077 | . 00012 | . 0001 |
| Square inches........ | 1273239. | 1000000. | ${ }^{645.2}$ | ${ }_{9}^{*} 6.452$ |  |  |  |  |
| Square feet............. |  | .............. | $\begin{array}{r} 92900 . \\ 836100 . \end{array}$ | $\begin{array}{r\|r} 929 . \\ 8361 . \end{array}$ | $\begin{array}{r} 144 . \\ 1296 . \end{array}$ | $\begin{aligned} & 1 . \\ & 9 . \end{aligned}$ | $.11111$ $1 .$ | $\begin{aligned} & .0929 \\ & * .836 \end{aligned}$ |
| Square yards.......... | ..... ......... | .................... | $\begin{array}{r} 836100 . \\ 1000000 . \end{array}$ | $\begin{array}{r\|r} 8361 . \\ 10000 . \end{array}$ | $\left\lvert\, \begin{array}{ll} 1 & 296 . \\ 1550.016 \end{array}\right.$ | $\underset{* 10.764}{9 .}$ | ${ }_{* 1.196}^{1 .}$ | 1. |

Circular mil = a circle whose diameter is .001 inch.
Square mil $=$ a square whose sides are .001 inch.
MEASURES OF VOLUME.

| Names of units. | Cubie centimeters. | Cubic inches. | Liters. | Gallons. | Cubic feet. | Cubic yards. | Cubic meters. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Cubic centimeters........ | 1. | *. 061 | . 001 | . 000264 | . 000035 | . 0000013 | . 000001 |
| Cubic inches ............... | *16.387 | 1. | . 016387 | . 00433 | . 000578 | .0000214 | . 000016 |
| Liters .......................... | 1000. | 61.023 | 1. | *. 26417 | . 035314 | . 001308 | . 001 |
| Gallons......................... | 3785.4 | 331. | *3.785 44 | 1. | .13368 | . 004952 | . 003785 |
| Cubic feet..................... | 28315. | 1728. | 28.315 |  |  |  |  |
| Cubic yards.................. | 764552. | 46656. | 764.55 | 201.97 | 27. | 1. | $\text { *. } 765$ |
| Cubic meters ............... | 1000000. | 61023. | 1000. | 264.17 | *35.314 | *1.308 |  |

Gallon $=4$ quarts.
Quart $=2$ pints.


MEASURES OF WORE.

| Names of units. | Ergs. |  | Pounddegree Fahrenheit. | Wattsecond. | Kilogrammeter. | Footpound. | Horse-powersecond. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Gram-degree Centigrade...... | 41549500. | 1. | . 0039683 | 4.15495 | . 42354 |  |  |
| Pound-degree Fahrenheit ..... | 10470300000. | 252.11 | 1. | 1047.03 | 106.731 | 772. | $1.403$ |
| Watt-second........................... | 10000000. | .2407 | . 0009551 | 1. | .101937 | .737324 | . 0013406 |
| Kilogram-meter . ... ............. | 98100000. | 2.361 | . 009369 | 9.81 | 1. | 7.23314 | . 013151 |
| Foot-pound............................. | 13562600. | . 3264 | . 0012953 | 1.35626 | ${ }^{1 .} 13825$ | 1. | . 00181818 |
| Horse-power-second ............. | $\ldots$ | 179.5 | . 7124 | 745.94 | 76.039 | 550. |  |

> Joule $=$ volt-coulomb $=$ watt for one second.
> Calorie $=$ gram-degree Centigrade.
> B. T. U. = British thermal unit $=$ pound-degree Fahrenheit.
MEASURES OF PRESSURE.

| Names of units. | Atmospheres. | Pounds on square inch. | Inches of mercury at $32^{\circ} \mathrm{F}$. | Feet of water at $60^{\circ} \mathrm{F}$. | Millimeters of mercury at $32^{\circ} \mathrm{F}$. | $\begin{gathered} \text { Pounds } \\ \text { on } \\ \text { square foot. } \end{gathered}$ | Kilograms on square meter. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Atmospheres.................................. | 1. | 14.7 | 29.922 | 33.94 | 760. | 2116. | 10333. |
| Pounds on square inch ............... | . 06803 | 1. | 2.036 | 2.309 | 51.7 | 143.946 | 702.925 |
| Inches of mercury at $32^{\circ} \mathrm{F}$........... | . 03342 | .4913 | 1. | 1.134 | 25.398 | 70.7 | 345.331 |
| Feet of water at $60^{\circ} \mathrm{F}$................ | . 02947 | . 4332 | . 8818 | 1. | 22.399 | 62.35 | 304.565 |
| Millimeters of mercury at $32^{\circ} \mathrm{F}$.... | . 001316 | . 01934 | . 03937 | . 04464 | 1 | 2.784 | 13.596 |
| Pounds on square foot................. | . 0004726 | . 006947 | . 01414 | . 01603 | . 3592 |  | 4.883 |
| Kilograms on square meter.......... | . 00009677 | . 001423 | . 002895 | . 003283 | . 07355 | . 2048 | 1. |

[^0]
## DECIMAL EQUIVALENTS OF PARTS OF AN INCH.

| 16ths. | 32ds. | 64ths. | Mils. | $16 \mathrm{ths}$. | 32ds. | 64ths. | Mils. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1 | $\begin{aligned} & 1 \\ & 2 \\ & 3 \\ & 4 \end{aligned}$ | $\begin{aligned} & 15.625 \\ & 31.25 \\ & 46.875 \\ & 62.5 \end{aligned}$ | 9 | 17 18 | $\begin{aligned} & 33 \\ & 34 \\ & 35 \\ & 36 \end{aligned}$ | 515.625 531.25 546.875 562.5 |
| 2 | 3 | $\begin{aligned} & 5 \\ & 6 \\ & 7 \\ & 8 \end{aligned}$ | $\begin{aligned} & 78.125 \\ & 93.75 \\ & 109.375 \\ & 125 . \end{aligned}$ | 10 | 19 20 | $\begin{aligned} & 37 \\ & 38 \\ & 39 \\ & 40 \end{aligned}$ | 578.125 593.75 609.375 625. |
| 3 | 5 6 | $\begin{array}{r} 9 \\ 10 \\ 11 \\ 12 \end{array}$ | $\begin{aligned} & 140.625 \\ & 156.25 \\ & 171.875 \\ & 187.5 \end{aligned}$ | 11 | 21 22 | 41 42 43 44 |  |
| 4 | 7 8 | $\begin{aligned} & 13 \\ & 14 \\ & 15 \\ & 16 \end{aligned}$ | 203.125 218.75 234.375 250. | 12 | 23 24 | 45 46 47 48 |  |
| 5 | ${ }^{9} 10$ | $\begin{aligned} & 17 \\ & 18 \\ & 19 \\ & 20 \end{aligned}$ | $\begin{aligned} & 265.625 \\ & 281.25 \\ & 296.875 \\ & 312.5 \end{aligned}$ | 13 | 25 26 | $\begin{aligned} & 49 \\ & 50 \\ & 51 \\ & 52 \end{aligned}$ | 765.625 781.25 796.875 812.5 |
| 6 | 11 12 | $\begin{aligned} & 21 \\ & 22 \\ & 23 \\ & 24 \end{aligned}$ | 328.125 343.75 359.375 375. | 14 | 27 28 | $\begin{aligned} & 53 \\ & 54 \\ & 55 \\ & 56 \end{aligned}$ | $\begin{aligned} & 828.125 \\ & 843.75 \\ & 859.375 \\ & 875 . \end{aligned}$ |
| 7 | 13 14 | $\begin{aligned} & 25 \\ & 26 \\ & 27 \\ & 28 \end{aligned}$ |  | 15 | 29 30 | $\begin{aligned} & 57 \\ & 58 \\ & 59 \\ & 60 \end{aligned}$ | 890.625 906.25 921.875 937.5 |
| 8 | 15 16 | $\begin{aligned} & 29 \\ & 30 \\ & 31 \\ & 32 \end{aligned}$ | $\begin{aligned} & 453.125 \\ & 468.75 \\ & 484.375 \\ & 500 . \end{aligned}$ | 16 | $\begin{aligned} & 31 \\ & 32 \end{aligned}$ | $\begin{aligned} & 61 \\ & 62 \\ & 63 \\ & 64 \\ & \hline \end{aligned}$ | $\begin{aligned} & 993.125 \\ & 968.75 \\ & 984.375 \\ & 1000 . \end{aligned}$ |

8 JOHN A. ROEBLING'S SONS $\mathbf{c o}$.

## WIRE GAUGES IN MILS.

| Numbers. | Roebling. | Brown \& Sharpe. | Birmingham or Stubs. | New British standard. |
| :---: | :---: | :---: | :---: | :---: |
| 000000 | 460. | ........* | ....... | 464. |
| 00000 | 430. | ......... | ....... | 432. |
| 0000 | 393. | 460. | 454. | 400. |
| 000 | 362. | 409.6 | 425. | 372. |
| 00 | 331. | 364.8 | 380. | 348. |
| 0 | 307. | 324.9 | 340. | 324. |
| 1 | 283. | 289.3 | 300. | 300. |
| 2 | 263. | 257.6 | 284. | 276. |
| 3 | 244. | 229.4 | 259. | 252. |
| 4 | 225. | 204.3 | 238. | 232. |
| 5 | 207. | 181.9 | 220. | 212. |
| 6 | 192. | 162. | 203. | 192. |
| 7 | 177. | 144.3 | 180. | 176. |
| 8 | 162. | 128.5 | 165. | 160. |
| 9 | 148. | 114.4 | 148. | 144. |
| 10 | 135. | 101.9 | 134. | 128. |
| 11 | 120. | 90.74 | 120. | 116. |
| 12 | 105. | 80.81 | 109. | 104. |
| 13 | 92. | 71.96 | 95. | 92. |
| 14 | 80. | 64.08 | 83. | 80. |
| 15 | - 72. | 57.07 | 72. | 72. |
| 16 | 63. | 50.82 | 65. | 64. |
| 17 | 54. | 45.26 | 58. | 56. |
| 18 | 47. | 40.3 | 49. | 48. |
| 19 | 41. | 35.89 | 42. | 40. |
| 20 | 35. | 31.96 | 35. | 36. |
| 21 | 32. | 28.46 | 32. | 32. |
| 22 | 28. | 25.35 | 28. | 28. |
| 23 | 25. | 22.57 | 25. | 24. |
| 24 | 23. | 20.1 | 22. | 22. |
| 25 | 20. | 17.9 | 20. | 20. |
| 26 | 18. | 15.94 | 18. | 18. |
| 27 | 17. | 14.2 | 16. | 16.4 |
| 28 | 16. | 12.64 | 14. | 14.8 |
| 29 | 15. | 11.26 | 13. | 13.6 |
| 30 | 14. | 10.03 | 12. | 12.4 |
| 31 | 13.5 | 8.93 | 10. | 11.6 |
| 32 | 13. | 7.95 | 9. | 10.8 |
| 33 | 11. | 7.08 | 8. | 10. |
| 34 | 10. | 6.8 | 7. | 9.2 |
| 35 | 9.5 | 5.62 | 5. | 8.4 |
| 36 | 9. | 5. | 4. | 7.6 |


| JOHN A. ROEBLING'S SONS CO. |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| WIRE GAUGES IN MILLIMETERS. |  |  |  |  |
| Numbers. | Roebling. | $\begin{aligned} & \text { Brown } \\ & \text { \& } \\ & \text { Sharpe. } \end{aligned}$ | $\begin{gathered} \text { Birmingham } \\ \text { or } \\ \text { Stubs. } \end{gathered}$ | New British standard. |
| $\begin{array}{r} 000000 \\ 00000 \\ 0000 \\ 000 \\ 00 \end{array}$ | 11.683 | ......... | ......... | 11.785 |
|  | 10.921 9.982 | 11.683 | 11.531 | 10.972 10.16 |
|  | 9.982 9.195 | 10.404 | 11.794 | 10.46 9.448 |
|  | 8.407 | 9.266 | 9.652 | 8.839 |
| $\begin{aligned} & 0 \\ & 1 \\ & 2 \\ & 3 \\ & 4 \end{aligned}$ | 7.798 | 8.251 | 8.636 | 8.229 |
|  | 7.188 6.68 | 7.348 | 7.62 | 7.62 |
|  | 6.68 6.198 | 6.544 5.827 | 7.213 6.579 | 6.401 |
|  | 5.715 |  | 6.045 | 5.893 |
| 56789 | 5.257 | 4.621 | 5.588 | 5.385 |
|  | 4.877 | 4.115 | 5.156 | 4.877 |
|  | 4.496 4.115 | 3.665 3.263 | 4.572 4.191 | 4.47 4.064 |
|  | 3.759 | 3.2006 | ${ }_{3.759}$ | 3.657 |
| $\begin{aligned} & 10 \\ & 11 \\ & 12 \\ & 13 \\ & 14 \end{aligned}$ | 3.429 | 2.588 | 3.404 | 3.251 |
|  | 3.048 2.667 | 2.305 2.052 | 3.048 2.768 | 2.947 2641 |
|  | 2.337 | 1.828 | 2.413 | 2.337 |
|  | 2.032 | 1.628 | 2.108 | 2.032 |
| $\begin{array}{r} 15 \\ -\quad 16 \\ 17 \\ 18 \\ 19 \end{array}$ | 1.829 | 1.449 | 1.829 | 1.829 |
|  | 1.6 1.372 | 1.291 1.15 | - $\begin{array}{r}1.651 \\ \hline\end{array}$ | 1.626 |
|  | 1.194 | 1.024 | 1.245 | 1.219 |
|  | 1.041 | . 9116 | 1.067 | 1.016 |
| $\begin{aligned} & 20 \\ & 21 \\ & 22 \\ & 23 \\ & 24 \end{aligned}$ | . 889 | . 8118 | . 889 | . 9144 |
|  | . 8128 | $\begin{array}{r}.7229 \\ 643 \\ \hline\end{array}$ | . 8128 | . 8128 |
|  | . 635 | . 6738 | . 6112 | . 6096 |
|  | . 5842 | . 5105 | . 5588 | . 5588 |
| 2526272829 | . 508 | . 4546 | . 508 | . 508 |
|  | .4572 | . 4049 | . 4572 | . 4572 |
|  | . 4318 | . 3605 | . 4064 | .4166 .375 |
|  |  |  |  |  |
| 3031323334 | . 3556 | . 2545 | . 3048 | . 315 |
|  | . 3429 | . 2267 | . 254 | . 2946 |
|  | .3302 .2794 | .2019 .179 | . 22286 | .274 8 |
|  | . 254 |  |  |  |
| 3536 | . 2413 | . 1426 |  | . 2134 |
|  | . 2286 | . 127 | . 1016 | . 193 |

## TABLES OF SPECIFIC GRAVITIES.

Metals.

| Names of metals. | Specific gravity. | Weights per cubic foot. | Specific heat. | Melting point in degrees Fahrenheit. |
| :---: | :---: | :---: | :---: | :---: |
| Aluminum, cast............ | $2.5{ }^{1}$ | 156.06 | . 2143 | ........* |
| "، hammered. | $2.67{ }^{1}$ | 166.67 |  | ........ |
| Antimony .................... | $6.702^{3}$ | 418.37 | . 0508 | 810. |
| Arsenic........................ | $5.763^{3}$ | 359.76 | . 0814 | 365. |
| Barium.......... ............... | $4 .{ }^{3}$ | 249.7 | ... | ........ |
| Bismuth...................... | $9.822^{2}$ | 613.14 | . 0308 | 497. |
| Cadmium .................... | $8.604^{5}$ | 537.1 | . 0567 | 500. |
| Calcium ....................... | $1.566^{4}$ | 97.76 | ........ | ........ |
| Chromium..................... | $7.3^{6}$ | 455.7 | 7107*********) | ...... |
| Cobalt ............................ | 8.6 | 536.86 | . 107 | ........ |
| Copper... ...................... | $8.895^{7}$ | 555.27 | . 0951 | 1996. |
| if rolled................. | $8.878^{2}$ | 554.21 | .......** | ........ |
| * cast.................... | $8.788{ }^{2}$ | 548.59 | ........* | ...... |
| * drawn................ | $8.9463^{8}$ | 558.47 | ........* | , |
| * hammered......... | $8.9587^{3}$ | 659.25 | ........ | ........ |
| " pressed. ........... | $8.931{ }^{\circ}$ | 55752 | ........ | ......** |
| " electrolytic........ | $8.914^{\text {c }}$ | 556.46 | ....... |  |
| Gold............................. | $19.258^{2}$ | 1202.18 | . 0324 | 2016. |
| Iron, bar...................... | $7.483^{\circ}$ | 467.18 | . 13 | 2786. |
| " wrought............... | 7.79 | 486.29 | . 113 | 3286. |
| Steel............................. | 7.85 | 490.03 | . 116 | 3286. |
| Lead.............................. | $11445{ }^{10}$ | 714.45 | . 0314 | 612. |
| Magncsinm.................. | $2.24{ }^{11}$ | 139.83 | .2499 | \%...... |
| Manganese.. ................ | ${ }_{6.912}$ | 430.73 | . 114 | 3000. |
| Mercury....................... | $13.568^{13}$ | 846.98 | . 0319 | -38. |
| Nickel .......................... | 7.832 | 488.91 | .1091 | 2800. |
| Platinum....................... | $20.3{ }^{2}$ | 1267.22 | . 0324 | 3286. |
| Potassium...................... | . $865^{14}$ | 54. | .1696 | 136. |
| Silver............................ | $10.522^{11}$ | 656.84 | . 057 | 1873. |
| Sodium......................... | . $972{ }^{14}$ | 60.68 | .2934 | 194. |
| Strontium................... | $2.504^{4}$ | 156.31 |  |  |
| Tin............................... | $7.291^{2}$ | 455.14 | . 0562 | 442. |
| Zinc ......................... .... | $6.861^{*}$ | 428.29 | . 0955 | 773. |

1. Wöhler.
2. Brisson.
3. Clarke.
4. Matthlessen.
5. Stromeyer.
6. Bunsen.
7. Hatchett.
8. Brezeníus.
9. Marchand \& Scheerer.
10. Musscheubroek.
11. Play fair \& Joule.
12. Bergman.
13. Watts' Dictionary.
14. Gay-Lussac \& Thenard.

## TABLES OF SPECIFIC GRAVITIES.-(Cont.)

 Liquids.| Names of liquids. | Specific gravity. | Temperatures. |
| :---: | :---: | :---: |
| Alcohol.. | 0.81571 | At $50^{\circ} \mathrm{F}$. |
| Benzine..................... ....... | 0.883 | At $59^{\circ} \mathrm{F}$. |
| Chloroform........................ | 1.491 | At $62.6{ }^{\circ} \mathrm{F}$. |
| Carbon bisulphide................ | 1.2931 | At $32^{\circ} \mathrm{F}$. |
| Ether......................... ........ | 0.7204 | At $60.8^{\circ} \mathrm{F}$. |
| Glycerine ......................... | 1.2636 | At $59{ }^{\circ} \mathrm{F}$. |
| Hydrochloric acid................. | 1.27 |  |
| Mercury ............................ | 13.596 | At $32^{\circ} \mathrm{F}$. |
| Nitric acid........................... | 1.552 | At $59^{\circ} \mathrm{F}$. |
| Oil of turpentine .................. | 0.855 to 0.864 | At $68{ }^{\circ} \mathrm{F}$. |
| Linseed oil......................... | 0.94 | ........ |
| Olive oil.............................. | 0.915 |  |
| Sulphuric acld...................... | 1.854 | At $32^{\circ} \mathrm{F}$. |

Gases.

| Names of gases. | At $0^{\circ} \mathrm{C}$. and 760 mm. pressure compared to water | At $0^{\circ} \mathrm{C}$. and 760 mm. pressure compared to air |
| :---: | :---: | :---: |
| Air... | 0.0012928 | 1. |
| Oxygen.... ......................... | 0.0014293 | 1.10563 |
| Nitrogen........................... | 0.0012557 | 0.97137 |
| Hydrogen..... ..................... | 0.00008954 | 0.06926 |
| Carbonic dioxide ................. | 0.0019767 | 1.5291 |
| Mixed gases from electro- lysis of water.................. | 0.0005861 | 0.41472 |
| Aqueous vapor ..................... | ................ | 0.623 |

## WEIGHTS OF SUBSTANCES.

| Names of substances. | Average weight per cubic foot. Pounds. |
| :---: | :---: |
| Aspbaltum........................................................ | 87. |
| Brick, common, hard.......................................... | 125. |
| Brickwork, pressed brick........................................................................... | 140. |
| Coal, anthracite, solid, of Penusylvania.................... | 112. 93. |
| " "6 broken, loose...................... ..... | 54. |
| " bituminous, solid................................................. | 84. |
| " ${ }^{\text {" }}$, broken; loose...... .................... | 49. |
| Coke, loose, of good coal...... ............................... | 62. |
| Cork........... .................................................. ... | 12.4 |
| Earth, common loam, dry, loose ........................ | 76. |
| " moderately rammed..... | 95. |
| Gneiss, common........ ..................................................... | 168. |
| Granite.............. | 170. |
| Glass, Crown................... ..................... ............. | 168.5 |
| " flint. | 218.3 |
| Ice at $0^{\circ} \mathrm{C}$. | 57.2 |
| Lime, thoroughly shaken.................................. | 755. |
| Masonry, of granite or limestone, well dressed | 165. |
| Mortar, hardened | 103. |
| Mud, dry, close. | 80 to 1 |
| Quartz.................................... ........................ | 165.4 |
| Sulphur. ................ ........................................... | 131.7 |
| Wax................................................................. | 58.7 |
| Wood, ebony... | 74.9 |
| " birch | 43.7 |
| " oak. | 46.8 |
| " pine | 31.2 |
| Water at $32^{\circ} \mathrm{F}$. | 62.418 |
| " " 39.1${ }^{\circ}$ F................................................. | 62.425 |
| " " $50^{\circ} \mathrm{F}$. | 62.409 |
| " " $60^{\circ} \mathrm{F}$.................. ............................... | 62.367 |
| " " $70^{\circ} \mathrm{F}$ | 62.302 |
| " " $80^{\circ} \mathrm{F}$. | 62.218 |
|  | 62.119 |

## THE COMPARISON OF THERMOMETERS．

Fahrenheit to Centigrade．
$\left(t^{\circ} \mathbf{F} .-32\right) \times{ }^{5}=$ Degrees $\mathbf{C}$ ．

|  |  | 高 |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 50 | 10. | 61 | 16.1 | 72 | 22.2 | 83 | 28.3 | 94 | 34.4 |
| 51 | 10.6 | 62 | 16.7 | 73 | 22.8 | 84 | 28.9 | 95 | 35. |
| 52 | 11.1 | 63 | 17.2 | 74 | 23.3 | 85 | 29.4 | 96 | 35.6 |
| 53 | 11.7 | 64 | 17.8 | 75 | 23.9 | 86 | 30. | 97 | 36.1 |
| 54 | 12.2 | 65 | 18.3 | 76 | 24.4 | 87 | 30.6 | 98 | 36.7 |
| 55 | 12.8 | 66 | 18.9 | 77 | 25. | 88 | 31.1 | 99 | 37.2 |
| 56 | 13.3 | 67 | 19.4 | 78 | 25.6 | 89 | 31.7 | 100 | 37.8 |
| 57 | 13.9 | 68 | 20. | 79 | 26.1 | 90 | 32.2 |  |  |
| 58 | 14.4 | 69 | 20.6 | 80 | 26.7 | 91 | 32.8 |  |  |
| 59 | 15. | 70 | 21.1 | 81 | 27.2 | 92 | 33.3 |  |  |
| 60 | 15.6 | 71 | 21.7 | 82 | 27.8 | 93 | 33.9 |  |  |

## Centigrade to Fahrenheit．

of ${ }^{\circ} \mathrm{C}+32=$ Degrees F ．

|  | $\begin{aligned} & \text { 苋 } \\ & \text { 品 } \\ & \text { H } \\ & \text { d } \\ & \text { ⿷匚 } \end{aligned}$ |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 10 | 50. | 18 | 64.4 |  | 78.8 | 34 | 93.2 |
| 11 | 51.8 | 19 | 66.2 | 27 | 80.6 | 35 | 95. |
| 12 | 53.6 | 20 | 68. | 28 | 82.4 | 36 | 96.8 |
| 13 | 55.4 | 21 | 69.8 | 29 | 84.2 | 37 | 98.6 |
| 14 | 57.2 | 22 | 71.6 | 30 | 86. | 38 | 100.4 |
| 15 | 59. | 23 | 73.4 | 31 | 87.8 | 39 | 10.2 |
| 16 | 60.8 | 24 | 75.2 | 32 | 89.6 | 40 | 104. |
| 17 | 62.6 | 25 | 77. | 33 | 91.4 |  |  |

## ELECTRICAL UNITS.

Final and offlial recommendation of the Chamber of Delegates of the International Electrical Congress, held at Chicago, 1893.

Resolved, That the several governments represented by the delegates of this International Congress of Electricians be, and they are hereby, recommended to formally adopt as legal units of electrical measure the following: As a unit of resistance, the international ohm, which is based upon the ohm equal to $10^{9}$ units of resistance of the C. G. S. system of electro-magnetic units, and is represented by the resistance offered to an unvarying electric current by a column of mercury at the temperature of melting ice 14.4521 grams in mass, of a constant cross-sectional area and of the length of 106.3 centimeters.

As a unit of current, the international ampere, which is one-tenth of the unit of current of the C. G. S. system of electro-magnetic units, and which is represented sufficiently well for practical use by the unvarying current which, when passed through a solution of nitrate of silver in water, and in accordance with accompanying specifications, ${ }^{1}$ deposits silver at the rate of 0.001118 of a gram per second.

[^1]As a unit of electro-motive force, the international volt, which is the electro-motive force that, steadily applied to a conductor whose resistance is one international ohm, will produce a current of one international ampere, and which is represented sufficiently well for practical use by $\frac{10}{1009}$ 年 of the electro-motive force between the poles or electrodes of the voltaic cell known as Clark's cell, at a temperature of $15^{\circ} \mathrm{C}$., and prepared in the manner described in the accompanying specification. ${ }^{2}$

As a unit of quantity, the international coulomb, which is the quantity of electricity transferred by a current of one international ampere in one second.

As a unit of capacity, the international farad, which is the capacity of a condenser charged to a potential of one international volt by one international coulomb of electricity.

As a unit of work, the joule, which is equal to $10^{7}$ units of work in the C. G. S. system, and which is represented sufficiently well for practical use by the energy expended in one second by an international ampere in an international ohm.

As a unit of power, the watt, which is equal to $10^{7}$ units of power in the C. G. S. system, and which is represented sufficiently well for practical use by work done at the rate of one joule per second.

As the unit of induction, the henry, which is the induction in a circuit when the electro-motive force induced in this circuit is one international volt, while the inducing current varies at the rate of one ampere per second.

[^2]
## COPPER WIRE.

I
N THE following tables of copper wire the value of the mil-foot is taken as the standard.
The temperature coëfficient is interpolated for $60^{\circ} \mathrm{F}$. and $75^{\circ} \mathrm{F}$. from the values given in the second table.

In the table for B. \& S. G., the actual sizes to which wire is drawn, are used.

In many cases the nearest whole number of pounds is taken when the variation is less than that found in actual weights of drawn wire.

In computing the weights, the specific gravity of copper is taken at 8.89 , water being at its greatest density 62.425 pounds per cubic foot.

International ohms are used, unless the kind of unit is specifically stated.

The following formulæ were used:

$$
\begin{aligned}
& \text { Resistance per } 1000 \text { feet at } 60^{\circ} \mathrm{F} .=\frac{10180.694}{\mathrm{~d}^{2}} \\
& \text { Resistance per } 1000 \text { feet at } 75^{\circ} \mathrm{F} .=\frac{10507.4}{\mathrm{~d}^{2} .} \\
& \text { Weight per } 1000 \text { feet }=.003027 \times \mathrm{d}^{2} . \\
& \text { Weight per mile }=.015983 \times \mathrm{d}^{2} .
\end{aligned}
$$

The following data and formulæ may be useful:
One B. A. unit $=.9889$ legal ohms $=.9866$ International ohms.
One legal ohm $=1.01122$ B. A. units $=.99767$ International ohms. One International ohm $=1.01358$ B. A. units $=1.00233$ legal ohms. One cubic foot of copper weighs 555 pounds. One cubic inch of copper weighs .3212 pounds.

$$
\begin{aligned}
& \text { Resistance per } 1000 \text { feet at } 60^{\circ} \mathrm{F} .=\frac{30.815}{\text { weight per } 1000 \text { feet. }} \\
& \text { Resistance per } 1000 \text { feet at } 75^{\circ} \mathrm{F} .=\frac{31.804}{\text { weight per } 1000 \text { feet. }}
\end{aligned}
$$

If a copper wire of length $l$, diameter $d$, and weight $w$, has a resistance $R$ at temperature $t$, then its conductivity
by diameter is given by the first formula, and by weight by the second.

$$
\begin{array}{ll}
C=\frac{a 1 k}{d^{2} R .} & R t^{\circ}=\frac{a 1 k}{d^{2}} \\
C=\frac{b l^{2} c}{w R .} & R t^{\circ}=\frac{b l^{2} c}{w .}
\end{array}
$$

Here, $a$ is the resistance of a mil-foot in same units as $R, k$ is the temperature coëfficient for $t^{\circ}$ Centigrade, and b is the resistance of one meter-gram at temperature $t^{\circ}$ and in same units as $R$.

> When 1 is in meters and $w$ in grams, $c=1$.
> When 1 isin feet and $w$ in grams, $c=.0929$.
> When 1 is in feet and $w$ in pounds, $c=.0002048$.

Mile-ohm $=$ weight per mile $\times$ resistance per mile.

$$
\begin{aligned}
& \text { Mile-ohm at } 60^{\circ}=859 \text {, International ohms. } \\
& \text { Mile-ohm at } 60^{\circ}=868.9, \text { B. A. units. } \\
& \text { Mile-ohm at } 60^{\circ}=861, \text { Legal ohms. }
\end{aligned}
$$

The following tables are taken from the report of the Standard Wiring Table Committee, published in the report of the meeting of the American Institute of Electrical Engineers, held January 17, 1893 :

## MATTHIESSEN'S STANDARD.

(Recommended by the Committee).

| Equivalent length of a square mm . mercury column. | B. A. units. | Legal ohms. | International ohms. |
| :---: | :---: | :---: | :---: |
|  | 104.8 cms . | 106.0 cms. | 106.3 cms . |
| Resistance at $0^{\circ} \mathbf{C}$. of Matthiessen's Standard-Meter-gram soft copper. | .14365.02057 | . 14206 |  |
|  |  |  | . 14173 |
| Meter-millimeter soft copper. |  | . 02035 | . 0203 |
| Cubic centimeter soft cop- |  |  |  |
| mil-foot soft copper.................................. | $9.000001616$ | $\begin{array}{r} .000001598 \\ 9.612 \end{array}$ | $\text { .000 } 001594$ |

## TEMPERATURE COËFFICIENTS.

Table of temperature variations in the resistance of pure soft copper according to Matthiessen's standard and formulæ.

|  |  |  | Matthiessen meter-gram standard resistance. |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | B. A. units. | Legal ohms. | International ohms. |
| 0 | 1. | 0. | 0.14365 | 0.14206 | 0.14173 |
| 1 | 1.003876 | 0.0016801 | 0.14421 | 0.14261 | 0.14228 |
| 2 | 1.007764 | 0.0033588 | 0.14477 | 0.14317 | 0.14283 |
| 3 | 1.01166 | 0.0050362 | 0.14533 | 0.14372 | 0.14338 |
| 4 | 1.01558 | 0.0067121 | 0.14589 | 0.14427 | 0.14394 |
| 5 | 1.0195 | 0.0083864 | 0.14645 | 0.14483 | 0.14449 |
| 6 | 1.02343 | 0.0100593 | 0.14702 | 0.14539 | 0.14505 |
| 7 | 1.02738 | 0.0117307 | 0.14759 | 0.14595 | 0.14561 |
| 8 | 1.03134 | 0.0134003 | 0.14815 | 0.14651 | 0.14617 |
| 9 | 1.03531 | 0.0150683 | 0.14873 | 0.14708 | 0.14673 |
| 10 | 1.03929 | 0.0167346 | 0.1493 | 0.14764 | 0.1473 |
| 11 | 1.04328 | 0.0183993 | 014987 | 0.14821 | 0.14786 |
| 12 | 1.04728 | 0.0200621 | 0.15045 | 0.14878 | 0.14843 |
| 13 | 1.05129 | 0.021723 | 0.15102 | 0.14935 | 0.149 |
| 14 | 1.05532 | 0.0233821 | 0.1516 | 0.14992 | 0.14957 |
| 15 | 1.05935 | 0.025039 | 0.15218 | 0.15049 | 0.15014 |
| 16 | 1.06339 | 0.026694 | 0.15277 | 0.15107 | 0.15071 |
| 17 | 1.06745 | 0.028348 | 0.15334 | 0.15164 | 0.15129 |
| 18 | 1.07152 | 0.029999 | 0.15393 | 0.15222 | 0.15186 |
| 19 | 1.07559 | 0.803164 | 0.15451 | 0.1528 | 0.15244 |
| 20 | 1.07968 | 0.033294 | 0.1551 | 0.15338 | 0.15302 |
| 21 | 1.08378 | 0.034939 | 0.15569 | 0.15396 | 0.1536 |
| 22 | 1.08788 | 0.036581 | 0.15628 | 0.15455 | 0.15418 |
| 23 | 1.092 | 0.038222 | 0.15687 | 0.15513 | 0.15477 |
| 24 | 1.09612 | 0.039859 | 0.15746 | 0.15572 | 0.15535 |
| 25 | - 1.10026 | 0.041494 | 0.15806 | 0.15631 | 0.15594 |
| 26 | 1.1044 | 0.043127 | 0.15865 | 0.15689 | 0.15653 |
| 27 | 1.10856 | 0.044758 | 0.15925 | 0.15748 | 0.15711 |
| 28 | 1.11272 | 0.046385 | 0.15985 | 0.15808 | 0.1577 |
| 29 | 1.11689 | 0.048011 | 0.16044 | 0.15867 | 0.1588 |
|  | 1.12107 | 0.049633 | 0.16105 | 0.15926 | 0.15889 |
| 40 | 1.16332 | 0.065699 | 0.16711 | 0.16526 | 0.16488 |
| 50 | 1.20625 | 0.081436 | 0.17328 | 0.17136 | 0.17095 |
| 60 | 1.24965 | 0.096787 | 0.17952 | 0.17753 | 0.17711 |
| 70 | 1.29327 | 0.111687 | 0.18578 | 0.18372 | 0.18329 |
| 80 | 1.33681 | 0.126069 | v. 19204 | 0.18991 | 0.18946 |
| 90 | 1.37995 | 0.139863 | 0.19823 | 0.19604 | 0.19558 |
| 100 | 142231 | 0.152995 | 0.20432 | 0.20206 | 0.20158 |

## PROPERTIES OF COPPER WIRE.

English system-Brown \& Sharpe gauge.

|  |  |  | Weights. |  | Resistances per 1000 feet in Interuational ohms. |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $\begin{aligned} & 1000 \\ & \text { feet. } \end{aligned}$ | Mile. | At $60^{\circ} \mathrm{F}$. | At $75^{\circ} \mathrm{F}$. |
| 0000 | 460. | 211600. | 641. | 3382. | . 04811 | . 04966 |
| 000 | 410. | 168100. | 509. | 2687. | . 06056 | . 06251 |
| 00 | 365. | 133225. | 403. | 2129. | . 07642 | . 07887 |
| 0 | 325. | 105625. | 320. | 1688. | . 09639 | . 09948 |
| 1 | 289. | 83521. | 253. | 1335. | . 1219 | . 1258 |
| 2 | 258. | 66564. | 202. | 1064. | . 1529 | . 1579 |
| 3 | 229. | 52441. | 159. | 838. | . 1941 | . 2004 |
| 4 | 204. | 41616. | 126. | 665. | . 2446 | . 2525 |
| 5 | 182. | 33124. | 100. | 529. | . 3074 | . 3172 |
| 6 | 162. | 26244. | 79. | 419. | . 3879 | . 4004 |
| 7 | 144. | 20736. | 63. | 331. | . 491 | . 5067 |
| 8 | 128. | 16384. | 50. | 262. | . 6214 | .6413 |
| 9 | 114. | 12996. | 39. | 268. | . 7834 | . 8085 |
| 10 | 102. | 10404. | 32. | 166. | . 9785 | 1.01 |
| 11 | 91. | 8281. | 25. | 132. | 1.229 | 1.269 |
| 12 | 81. | 6561. | 20. | 105. | 1.552 | 1.601 |
| 13 | 72. | 5184. | 15.7 | 83. | 1.964 | 2.027 |
| 14 | 64. | 4096. | 12.4 | 65. | 2.485 | 2.565 |
| 15 | 57. | 3249. | 9.8 | 52. | 3.133 | 3.234 |
| 16 | 51. | 2601. | 7.9 | 42. | 3.914 | 4.04 |
| 17 | 45. | 2025. | 6.1 | 32. | 5.028 | 5.189 |
| 18 | 40. | 1600. | 4.8 | 25.6 | 6.363 | 6.567 |
| 19 | 36. | 1296. | 3.9 | 20.7 | 7.855 | 8.108 |
| 20 | 32. | 1024. | 3.1 | 16.4 | 9.942 | 10.26 |
| 21 | 28.5 | 812.3 | 2.5 | 13. | 12.53 | 12.94 |
| 22 | 25.3 | 640.1 | 1.9 | 10.2 | 15.9 | 16.41 |
| 23 | 22.6 | 510.8 | 1.5 | 8.2 | 19.93 | 20.57 |
| 24 | 20.1 | 404. | 1.2 | 6.5 | 25.2 | 26.01 |
| 25 | 17.9 | 320.4 | . 97 | 5.1 | 31.77 | 32.79 |
| 26 | 15.9 | 252.8 | . 77 | 4. | 40.27 | 41.56 |
| 27 | 14.2 | 201.6 | . 61 | 3.2 | 50.49 | 52.11 |
| 28 | 12.6 | 158.8 | . 48 | 2.5 | 64.13 | 66.18 |
| 29 | 11.3 | 127.7 | . 39 | 2. | 79.73 | 82.29 |
| 30 | 10. | 100. | . 3 | 1.6 | 101.8 | 105.1 |
| 31 | 8.9 | 79.2 | . 24 | 1.27 | 128.5 | 132.7 |
| 32 | 8. | 64. | . 19 | 1.02 | 159.1 | 164.2 |
| 33 | 7.1 | 50.4 | . 15 | . 81 | 202. | 208.4 |
| 34 | 6.3 | 39.7 | . 12 | . 63 | 256.5 | 264.7 |
| 35 | 5.6 | 31.4 | . 095 | . 5 | 324.6 | 335.1 |
| 36 | 5. | 25. | . 076 | . 4 | 407.2 | 420.3 |

## PROPERTIES OF COPPER WIRE.-(Cont.)

English system-Birmingham wire gavge.

|  |  |  | Weights. |  | Resistances per 1000 feet in International ohms. |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $\begin{aligned} & 1000 \\ & \text { feet. } \end{aligned}$ | Mile. | At $60^{\circ} \mathrm{F}$. | At $75^{\circ} \mathrm{F}$. |
| 0000 | 454. | 206116. | 624. | 3294. | . 04939 | . 05098 |
| 000 | 425. | 180625. | 547. | 2887. | . 05636 | . 05817 |
| 00 | 380. | 144400. | 437. | 2308. | . 0705 | . 07277 |
| 0 | 340. | 115600. | 350. | 1817. | . 08807 | . 09089 |
| 1 | 300. | 90000. | 272. | 1438. | . 1131 | . 1167 |
| 2 | 284. | 80656. | 244. | 1289. | .1262 | . 1303 |
| 3 | 259. | 67081. | 203. | 1072. | . 1518 | . 1566 |
| 4 | 238. | 56644. | 171. | 905. | . 1797 | . 1855 |
| 5 | 220. | 48400. | 146. | 773. | .2103 | . 2171 |
| 6 | 203. | 41209. | 125. | 659. | . 2471 | . 255 |
| 7 | 180. | 32400. | 98. | 518. | . 3142 |  |
| 8 | 165. | 27225. | 82 | 435. | . 8739 | . 3859 |
| 9 | 148. | 21904. | 66. | 350. | . 4648 | . 4797 |
| 10 | 134. | 17956. | 54. | 287. | . 567 | . 5852 |
| 11 | 120. | 14400. | 44. | 230. | . 707 | . 7297 |
| 12 | 109. | 11881. | 36. | 190. | . 8569 | . 8844 |
| 13 | 95. | 9025. | 27.3 | 144. | 1.128 | 1.164 |
| 14 | 83. | 6889. | 20.8 | 110. | 1.478 | 1.525 |
| 15 | 72. | 5184. | 15.7 | 83. | 1.964 | 2.027 |
| 16 | 65. | 4225. | 12.8 | 68. | 2.41 | 2.487 |
| 17 | 58. | 3364. | 10.2 | 54 | 3.026 | 3.123 |
| 18 | 49. | 2401. | 7.3 | 38.4 | 4.24 | 4.376 |
| 19 | 42. | 1764. | 5.3 | 28.2 | 5.771 | 5.957 |
| 21 | 35. | 1225. | 3.7 | 19.6 | - 8.311 | 8.577 |
| 21 | 32. | 1024. | 3.1 | 16.4 | 9.942 | 1026 |
| 22 | 28. | 784. | 2.4 | 12.5 | 12.99 | 13.4 |
| 23 | 25. | 625. | 1.9 | 10. | 16.29 | 16.81 |
| 24 | 22. | 484. | 1.5 | 7.7 | 21.03 | 21.71 |
| 25 | 20. | 400. | 1.2 | 6.4 | 25.45 | 26.27 |
| 26 | 18. | 324. | . 98 | 52 | 31.42 | 32.43 |
|  | 16. |  |  | 4.1 | 39.77 | 41.04 |
| 28 | 14. | 196. | . 59 | 3.1 | 51.94 | 53.61 |
| 29 | 13. | 169. | . 51 | 2.7 | 60.24 | 62.17 |
| 30 | 12. | 144. | . 44 | 2.3 | 70.7 | 72.97 |
| 31 | 10. | 100. | . 3 | 1.6 | 108. | 105.1 |
|  | 9. | 81. | . 25 | 1.3 | 125.7 | 129.7 |
| 33 | 8. | 64. | .19 | 1.02 | 159.1 | 164.2 |
| 34 | 7. | 49. | . 15 | . 78 | 207.8 | 214.4 |
| 35 | 5. | 25. | . 075 | .4 | 407.2 | 420.3 |
| 36 | 4. | 16. | . 048 | 256 | 636.3 | 656.7 |

## PROPERTIES OF COPPER WIRE.-(Cont.)

English system-New British standard gange.

| $\begin{aligned} & \text { 总 } \\ & \text { 曾 } \\ & \frac{\square}{4} \end{aligned}$ |  |  | Weights. |  | Resistances per 1000 feet in International ohms. |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $\begin{aligned} & 1000 \\ & \text { feet. } \end{aligned}$ | Mile. | At $60^{\circ} \mathrm{F}$. | At $75^{\circ} \mathrm{F}$. |
| 000000 | 464. | 215296. | 652. | 3441. | . 04729 | . 0488 |
| 00000 | 432. | 186624. | 565. | 2983. | . 05455 | . 0563 |
| 0000 | 400. | 160000. | 484. | 2557. | . 06363 | . 06567 |
| 000 | 372 | 138384. | 419. | 2212. | . 07357 | . 07593 |
| 00 | 348. | 121104. | 367. | 1935. | . 08407 | . 08676 |
| 0 | 324. | 104976. | 318. | 1678. | . 9698 | . 10009 |
|  | 300. | 90000. | 272. | 1438. | . 1131 | . 1167 |
| 2 | 276. | 76176. | 231. | 1217. | . 1336 | . 1379 |
| 3 | 252. | 63504. | 192. | 1015. | . 1603 | . 1655 |
| 4 | 232. | 53824. | 163. | 860. | . 1892 | . 1952 |
| 5 | 212. | 44914. | 136. | 718. | . 2265 | . 2338 |
| 6 | 192. | 36864. | 112. | 589. | . 2762 | . 285 |
| 7 | 176. | 30976. | 94. | 495. | . 3287 | . 3392 |
| 8 | 160. | 25600. | 77. | 409. | . 3977 | . 4104 |
| 9 | 144. | 20736. | 63. | 331. | . 491 | . 5067 |
| 10 | 128. | 16384. | 50. | 262. | . 6214 | . 6413 |
| 11 | 116. | 13456. | 41. | 215. | . 7566 | . 7809 |
| 12 | 104. | 10816. | 33. | 173. | .9413 | . 9715 |
| 13 | 92. | 8464. | 25.6 | 135. | 1. 203 | 1.241 |
| 14 | 80. | 6400. | 19.4 | 102. | 1.591 | 1.642 |
| 15 | 72. | 5184. | 15.7 | 83. | 1.964 | 2.027 |
| 16 | 64. | 4096. | 12.4 | 65. | 2.486 | 2.565 |
| 17 | 56. | 3136. | 9.5 | 50. | 3.246 | 3.351 |
| 18 | 48. | 2304. | 7. | 36.8 | 4.419 | 4.561 |
| 19 | 40. | 1600. | 4.8 | 25.6 | 6.363 | 6.567 |
| 20 | 36. | 1296. | 3.9 | 20.7 | 7.855 | 8.108 |
| 21 | 32. | 1024. | 3.1 | 16.4 | 9.942 | 10.26 |
| 22 | 28. | 784. | 2.4 | 12.5 | 12.99 | 13.4 |
| 23 | 24. | 576. | 1.7 | 9.2 | 17.67 | 18.24 |
| 24 | 22. | 484. | 1.5 | 7.7 | 21.03 | 21.71 |
| 25 | 20. | 400. | 1.2 | 6.4 | 25.45 | 26.27 |
| 26 | 18. | 324. | . 98 | 5.2 | 31.42 | 32.43 |
| 27 | 16.4 | 269. | . 81 | 4.3 | 37.85 | 39.07 |
| 28 | 14.8 | 219. | . 66 | 8.5 | 46.48 | 47.97 |
| 29 | 13.6 | 185. | . 56 | 3. | 55.04 | 56.81 |
| 30 | 12.4 | 153.8 | . 47 | 2.5 | 66.21 | 68.34 |
| 81 | 11.6 | 134.6 | . 41 | 2.15 | 75.66 | 78.09 |
| 32 | 10.8 | 116.6 | . 35 | 1.86 | 87.28 | 90.08 |
| 33 | 10. | 100. | . 3 | 1.6 | 101.8 | 105.1 |
| 34 | 9.2 | 84.6 | . 26 | 1.35 | 120.3 | 124.1 |
| 35 | 8.4 | 70.6 | . 21 | 1.13 | 144.3 | 148.9 |
| 36 | 7.6 | 57.8 | . 17 | . 92 | 176.3 | 181.9 |

## PROPERTIES OF COPPER WIRE.-(Cont.)

Metric system-Brown \& Sharpe gauge.

| $\begin{aligned} & \text { 韋 } \\ & \text { 8 } \\ & \text { 总 } \\ & \text { Z } \end{aligned}$ |  |  |  | Resistances per kilometer in International ohms. |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | At $60^{\circ} \mathrm{F}$. | At $75^{\circ} \mathrm{F}$. |
| 0000 | 11.683 | 107.2 | 954.3 | .1578 | . 1629 |
| 000 | 10.404 | 85.01 | 756.8 | . 1987 | . 2051 |
| 00 | 9.266 | 67.43 | 600.2 | . 2507 | . 2588 |
| 0 | 8.251 | 53.47 | 480.4 | . 3162 | . 3264 |
| 1 | 7.348 | 42.41 | 377.4 | . 3999 | . 4127 |
| 2 | 6.544 | 33.63 | 299.3 | . 5018 | . 5179 |
| 3 | 5.827 | 26.67 | 237.4 | . 6369 | . 6574 |
| 4 | 5.19 | 21.16 | 188.3 | . 8026 | . 8284 |
| 5 | 4.621 | 16.77 | 149.3 | 1.009 | 1.041 |
| 6 | 4.115 | 13.3 | 118.4 | 1.273 | 1.314 |
| 7 | 3.665 | 10.55 | 93.9 | 1.611 | 1.662 |
| 8 | 3.263 | 8.362 | 74.5 | 2.039 | 2.104 |
| 9 | 2.906 | 6.633 | 59. | 2.57 | 2.653 |
| 10 | 2.588 | 5.26 | 46.8 | 3.21 | 3.313 |
| 11 | 2.305 | 4.173 | 37.1 | 4.033 | 4.163 |
| 12 | 2.052 | 3.307 | 29.5 | 5.091 | 5.253 |
| 13 | 1.828 | 2.625 | 23.4 | 6.443 | 6.65 |
| 14 | 1.628 | 2.082 | 18.5 | 8.155 | 8.416 |
| 15 | 1.449 | 1.649 | 14.7 | 10.28 | 10.61 |
| 16 | 1.291 | 1.309 | 11.7 | 12.84 | 13.25 |
| 17 | 1.15 | 1.039 | 9.23 | 16.5 | 17.02 |
| 18 | 1.024 | . 8236 | 7.32 | 20.88 | 21.55 |
| 19 | . 9116 | . 6527 | 5.8 | 25.77 | 26.6 |
| 20 | . 8118 | . 5176 | 4.61 | 32.62 | 33.66 |
| 21 | .7229 | .4104 | 3.65 | 41.11 | 42.45 |
| 22 | . 6438 | . 3255 | 2.89 | 52.16 | 53.84 |
| 23 | . 5733 | . 2581 | 2.16 | 65.39 | - 67.49 |
| 24 | . 5105 | . 2047 | 1.82 | 82.68 | 85.33 |
| 25 | . 4546 | . 1623 | 1.44 | 104.2 | 107.6 |
| 26 | . 4049 | . 1288 | 1.15 | 132.1 | 136.3 |
| 27 | .8605 | .1021 | . 908 | 165.1 | 171. |
| 28 | . 3211 | . 081 | . 72 | 210.4 | 217.1 |
| 29 | . 2859 | . 0642 | . 572 | 261.6 | 270. |
| 30 | . 2545 | . 0509 | . 452 | 334. | 344.8 |
| 31 | . 2267 | . 0404 | . 359 | 421.6 | 435.4 |
| 32 | .2019 | . 032 | . 284 | 522. | 538.7 |
| 33 | . 1798 | . 0254 | . 226 | 662.7 | 683.7 |
| 34 | . 1601 | . 0201 | . 179 | 841.5 | 868.4 |
| 35 | . 1426 | . 016 | . 141 | 1065. | 1099. |
| 36 | . 127 | . 0127 | . 113 | 1336. | 1379. |

## WEIGHTS OF COPPER WIRE.

Metric system-per kilometer, in kilograms.

| Numbers. | Roebling. | Brown \& Sharpe. | Birmingham or Stubs. | New British standard. |
| :---: | :---: | :---: | :---: | :---: |
| 000000 | 954.3 | ......... | ........* | 970.9 |
| 00000 | 833.9 | *....... | ........ | 841.6 |
| 0000 | 696.5 | 954.3 | 929.4 | 721.5 |
| 000 | 591. | 756.8 | 814.5 | 624. |
|  | 494.1 | 600.2 | 651.3 | 546.2 |
| 0 | 425.1 | 480.4 | 521.3 | 473.4 |
| 1 | 361.2 | 377.4 | 405.8 | 405.8 |
| 2 | 311.9 | 299.3 | 363.3 | 343.5 |
| 3 | 268.5 | 237.4 | 302.6 | 286.3 |
| 4 | 228.3 | 188.3 | 255.3 | -242.7 |
| 5 | 193.2 | 149.3 | 218.3 | 202.7 |
| 6 | 166.2 | 118.4 | 185.9 | 166.2 |
| 7 | 141.3 | 93.9 | 146.1 | 139.7 |
| 8 | 118.3 | 74.5 | 122.8 | 115.4 |
| 9 | 98.8 | 59. | 98.8 | 93.5 |
| 10 | 82.2 | 46.8 | 81. | 78.9 |
| 11 | 64.9 | 37.1 | 64.9 | 60.7 |
| 12 | 49.9 | 29.5 | 53.6 | 48.8 |
| 13 | 38.2 | 23.4 | 39.8 | 38.2 |
| 14 | 28.9 | 18.5 | 31.1 | 28.9 |
| 15 | 23.4 | 14.7 | 23.4 | 23.4 |
| 16 | 17.9 | 11.7 | 19.1 | 18.5 |
| 17 | 13.2 | 9.23 | 15.2 | 14.1 |
| 18 | 9.96 | 7.32 | 10.8 | 10.4 |
| 19 | 7.58 | 5.8 | 7.95 | 7.22 |
| 20 | 5.52 | 4.61 | 5.52 | 5.85 |
| 21 | 4.61 | 3.65 | 4.62 | 4.61 |
| 22 | 3.54 | 2.89 | 3.54 | 3.54 |
| 23 | 2.81 | 2.16 | 2.81 | 2.59 |
| 24 | 2.38 | 1.82 | 2.19 | 2.19 |
| 25 | 1.8 | 1.44 | 1.8 | 1.8 |
| 26 | 1.46 | 1.15 | 1.46 | 1.46 |
| 27 | 1.3 | . 908 | 1.16 | 1.21 |
| 28 | 1.15 | . 72 | . 884 | . 988 |
| 29 | 1.02 | . 572 | . 762 | . 833 |
| 30 | . 884 | . 452 | . 649 | . 694 |
| 31 | . 822 | . 359 | . 451 | . 607 |
| 32 | . 762 | . 284 | . 365 | . 525 |
| 33 | . 544 | . 2226 | . 289 | . 451 |
| 34 | . 451 | . 179 | . 22 | . 381 |
| 35 | .406 | . 141 | . 113 | . 319 |
| 36 | . 365 | . 113 | . 071 | . 26 |

## HARD-DRAWN COPPER WIRE.

British Post-office specifications.

"The wire shall be capable of being wrapped in six turns around wire of its own diameter, unwrapped and again wrapped in six turns around wire of its own diameter in the same direction as the first wrapping, without breaking; and shall be also capable of bearing the number of twists set down in the table, without breaking.
"The twist-test will be made as follows: The wire will be gripped by two vises, one of which will be made to revolve at a speed not exceeding one revolution per second. The twists thus given to the wire will be reckoned by means of an ink mark which forms a spiral on the wire during torsion, the full number of twists to be visible between the vises."

According to the above table, the mile-ohm of copper required is 878 pounds. This corresponds to a conductivity of 96.6 per cent., taking the value of the mile-ohm of 100 per cent. copper as 859 .
HARD－DRAWN COPPER WIRE．－（Continued．）

| Numbers． | Diameters in mils． |  |  | Weights per mile． |  |  | Breaking weights． |  |  | Weights of coils． |  | Conduc－ tivity． |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $\begin{aligned} & \text { 者 } \\ & \text { 品 } \\ & \end{aligned}$ |  | 見 |  |  | $\begin{aligned} & \text { 플 } \\ & \text { 苐 } \\ & \text { 品 } \end{aligned}$ |  | 关 悲 感 | $\begin{aligned} & \text { 品 } \\ & \text { 豆 } \\ & \text { ㄹ } \end{aligned}$ |  | $\begin{aligned} & \text { gi } \\ & \text { 品 } \\ & \text { 员 } \end{aligned}$ |  |  |
| 8 B．W．G．．．．．．． | 165. | 166. | 164. | 436.4 | 441.7 | 431.1 | 1328 | 1301 | 62100 | 218 | 152 | 97 | 96 | 30 | 1.14 |
| $12 \mathrm{~N} . \mathrm{B} . \mathrm{S} . \mathrm{G}$. ， | 104. | 104.9 | 103.1 | 173.4 | 176.4 | 170.4 | 549 | 538 | 64600 | 219 | 151 | 97 | 96 | 40 | 1. |
| $10 \mathrm{~B} . \&$ S．G．．． | 101.9 | 102.8 | 101. | 165. | 168. | 162. | 540 | 519 | 64800 | 218 | 152 | 97 | 96 | 40 | ． 99 |
| 12 B．\＆S．G．．． | 80. | 81.2 | 79.3 | 102.6 | 105.7 | 100.8 | 334 | 327 | 66500 | 72 | 52 | 97 | 96 | 44 | ． 94 |
| 14 B．\＆S．G．．． | 64. | 65. | 63. | 65. | 67.5 | 63. | 220 | 212 | 68200 | ．．．．． | ．．．．． | 97 | 96 | 47 | ． 91 |

## TENSILE STRENGTH OF COPPER WIRE.

| Numbers, B. \& S. G. | Breaking weight. Pounds. |  | Numbers, <br> B. \& S. G. | Breaking weight. Pounds. |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Harddrawn. | Annealed. |  | Harddrawn. | $\underset{\text { An- }}{\text { nealed. }}$ |
| 0000 | 8310 | 5650 | 9 | 617 | 349 |
| 000 | 6580 | 4480 | 10 | 489 | 277 |
| 00 | 5226 | 3553 | 11 | 388 | 219 |
| 0 | 4558 | 2818 | 12 | 307 | 174 |
| 1 | 3746 | 2234 | 13 | 244 | 138 |
| 2 | 3127 | 1772 | 14 | 193 | 109 |
| 3 | 2480 | 1405 | 15 | 153 | 87 |
| 4 | 1967 | 1114 | 16 | 133 | 69 |
| 5 | 1559 | 883 | 17 | 97 | 55 |
| 6 | 1237 | 700 | 18 | 77 | 43 |
| 7 | 980 | 555 | 19 | 61 | 34 |
| 8 | 778 | 440 | 20 | 48 | 27 |

The strength of soft copper wire varies from 32000 to 36000 pounds per square inch, and of hard copper wire from 45000 to 68000 pounds per square inch, according to the degree of hardness.

The above table is calculated for 34000 pounds for soft wire and 60000 pounds for hard wire, except for some of the larger sizes, where the breaking weight per square inch is taken at 50000 pounds for 0000,000 and 00,55000 for 0 , and 57000 pounds fur 1 .

## BI-METALLIC WIRE.

| Numbers, <br> B. \& S. G. | Diameters <br> in mils. | Weights per <br> mile. <br> Pounds. | Breaking weight. <br> Pounds. |
| :---: | :---: | :---: | :---: |
| 0000 | 460 | 3200 | $10500^{\circ}$ |
| 000 | 410 | 2537 | 8600 |
| 00 | 365 | 2022 | 7000 |
| 0 | 325 | 1620 | 5700 |
| 1 | 289 | 1264 | 4600 |
| 2 | 258 | 1003 | 3800 |
| 3 | 229 | 797 | 3200 |
| 4 | 204 | 629 | 2600 |
| 5 | 182 | 490 | 1790 |
| 6 | 162 | 398 | 1500 |
| 7 | 144 | 314 | 1210 |
| 8 | 128 | 246 | 1020 |
| 9 | 114 | 203 | 850 |
| 10 | 102 | 157 | 660 |
| 11 | 91 | 127 | 520 |
| 12 | 81 | 100 | 410 |
| 14 | 64 | 63 | 260 |
| 16 | 51 | 40 | 160 |
| 18 | 40 | 25 | 100 |

This wire consists of a steel center with a cover of copper. Its conductivity is about 65 per cent. of that of pure copper. The percentage of copper and steel may vary a trifle, hence the strength and weight must be approximate.

## STRANDS OF COPPER WIRE.

COPPER WIRES are laid up into concentric strands or into ropes of seven strands. A rope of seven strands each composed of seven wires, is called a seven by seven rope, and is usually written $7 \times 7$. The number of wires that can be made into a strand is limited by the capacity of the stranding machinery. Two hundred wires is the usual limit of a concentric strand, and one hundred and thirty-three wires of a rope.

In a strand of circular milage, C. M., composed of $n$ wires of diameter d, with a weight per 1000 feet $w$, then we have

$$
\text { C. } \begin{aligned}
\mathrm{M} . & =\mathrm{d}^{2} \times \mathrm{n} . \\
\mathrm{n} & =\frac{\mathrm{C} \cdot \mathrm{M} .}{\mathrm{d}^{2}} \\
\mathrm{~d} & =\sqrt{\frac{\mathrm{C} \cdot \mathrm{M}}{\mathrm{n}}} \\
\mathrm{w} & =.00305 \times \mathrm{C} . \mathrm{M} .
\end{aligned}
$$

The weights of strands are calculated about one per cent. heavier than a solid wire of the same circular milage, while the resistance is calculated for the solid wire.

In specifying how a strand shall be made, the number of wires to be used or the diameter of each wire may be given. In the first case the wire usually has to be specially drawn, and this will delay an order, especially a small order, unduly. It is, therefore, better to specify the size wires B. \&. S. G., of which the strand is to be made.

The diameter of a strand may be calculated by multiplying the dianeter of one wire by the factors given in the table at the bottom of the opposite page, according to the number of wires composing the strand.

## STRANDS OF COPPER WIRE.

Diameters and properties.

|  | Circular mils. | Diameters. |  | Weights. |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Decimal parts of inch. | $\begin{gathered} \text { Nearest } \\ 32 \mathrm{~d} . \end{gathered}$ | $\begin{aligned} & 1000 \\ & \text { feet. } \end{aligned}$ | Mile. |  |
| ........ | 1000000 | 1.152 | $1 \frac{3}{16}$ | 3050 | 16104 | . 01051 |
| ........ | 950000 | 1.125 | 11/8 | 2898 | 15299 | . 01106 |
| ........ | 900000 | 1.092 | $1{ }^{31}$ | 2745 | 14494 | . 01167 |
| ........ | 850000 | 1.062 | $1 \frac{1}{18}$ | 2593 | 13688 | . 01236 |
| ........ | 800000 | 1.035 | $1 \frac{1}{31}$ | 2440 | 12883 | . 01313 |
| ... | 750000 | . 999 | 1 | 2288 | 12078 | . 01401 |
| .... | 700000 | . 963 | ${ }^{3}$ | 2135 | 11273 | . 01501 |
| ........ | 650000 | . 927 | $\frac{15}{18}$ | 1983 | 10468 | :016 17 |
| ........ | 600000 | . 891 | 弱 | 1830 | 9662 | . 01751 |
| ........ | 550000 | . 855 | 7/8 | 1678 | 8857 | . 0191 |
| ........ | 500000 | . 819 | 18 | 1525 | 8052 | . 02101 |
| ....... | 450000 | . 770 | $\frac{35}{5}$ | 1373 | 7247 | . 02335 |
| ........ | 400000 | . 728 | 3/4 | 1220 | 6442 | . 02627 |
| ........ | 350000 | . 679 | 118 | 1068 | 5636 | . 03002 |
| $\ldots$ | 300000 | . 630 | 5/8 | 915 | 4831 | . 03502 |
|  | 250000 | . 590 | ${ }^{\frac{19}{2}}$ | 762 | 4026 | . 04203 |
| 0000 | 211600 | . 530 | ${ }_{17} \frac{1}{2}$ | 645 | 3405 | . 04966 |
| 000 | 168100 | . 470 | 㗣 | 513 | 2709 | . 06251 |
| 00 | 133225 | . 420 | ${ }^{70}$ | 406 | 2144 | . 07887 |
| 0 | 105625 | . 375 | 8/8 | 322 | 1700 | . 09948 |
| 1 | 83521 | . 330 | 3 | 255 | 1346 | . 1258 |
| 2 | 66564 | 291 | ${ }^{18}$ | 203 | 1072 | . 1579 |
| 3 | 52441 | . 261 | $\frac{8}{37}$ | 160 | 845 | . 2004 |
| 4 | 41616 | . 231 | 1/4 | 127 | 671 | . 2525 |


| Numbers of <br> wires. | Factors. | Numbers of <br> wires. | Factors. |
| :---: | :---: | :---: | :---: |
| 3 | $21 / 4$ | 75 |  |
| 7 | 3 | 91 | $101 / 4$ |
| 12 | $41 / 4$ | 108 | 11 |
| 19 | 5127 | $121 / 4$ |  |
| 27 | $61 / 4$ | 147 | 13 |
| 37 | 7 | 169 | $141 / 4$ |
| 48 | $81 / 4$ | 192 | 15 |
| 61 | 9 | 217 | $161 / 4$ |
| $7 \times 7$ | 9 | $\ldots .$. | 17 |
| $7 \times 19$ | 15 | $\ldots .$. |  |


NUMBERS OF WIRES IN STRANDS.

| a | Numbers, Brown \& Sharpe gaug |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 8 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 22 | 25 | 28 | 30 | B. $12 \mathrm{~N} . \mathrm{G}$. |
|  | Number of wires in strands. |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1000000 950000 800000 800000 | 61. <br> $\stackrel{58}{54.9}$ <br> 51.9 48.8 | 96.191.386.581.776.9 | $\begin{gathered} 120.8 \\ 114.8 \\ 108.7 \\ 102.7 \\ 96.6 \end{gathered}$ | $\begin{aligned} & 152.4 \\ & 144.8 \\ & 137.2 \\ & 129.5 \\ & 121.9 \end{aligned}$ | $\begin{aligned} & 192.9 \\ & 183.2 \\ & 173.6 \\ & 164.6 \\ & 154.3 \end{aligned}$ | $\begin{aligned} & 244.1 \\ & 23.9 \\ & 219.7 \\ & 207.5 \\ & 195.3 \end{aligned}$ | $\begin{aligned} & 307.8 \\ & 292.4 \\ & 277 . \\ & 271.6 \\ & 246.2 \end{aligned}$ | 384.5 <br> 365.3 <br> 346.1 <br> 326.8 <br> 307.6 | 493.8 <br> 469.1 <br> 44.5 <br> 419.8 <br> 395.1 | $500 .$ | $\begin{aligned} & 771.6 \\ & 73.6 \\ & 69.4 \\ & 655.9 \\ & 617.3 \\ & \hline \end{aligned}$ | $\begin{aligned} & 976.6 \\ & 927.8 \\ & 878.9 \\ & 83.9 \\ & 781.3 \end{aligned}$ | $\begin{aligned} & 1562 . \\ & 148 . \\ & 140 . \\ & 1432 . \\ & 1250 . \end{aligned}$ | $\begin{aligned} & 3121 . \\ & 2965 . \\ & 22_{2} 89 . \\ & 2653 . \\ & 265 . \\ & 2497 . \\ & \hline \end{aligned}$ | 6299.59845669.5354.5039. | $\begin{array}{r} 10000 . \\ 9500 \\ 9000 \\ 95500 \\ 8000 \\ 8000 . \end{array}$ | $\begin{aligned} & 92.5 \\ & 87.9 \\ & 88.8 \\ & 76 . \end{aligned}$ |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | $\begin{aligned} & 45.8 \\ & 42.7 \\ & 39.7 \\ & 366 \\ & 33.6 \end{aligned}$ | $\begin{aligned} & 72.1 \\ & 67.3 \\ & 62.5 \\ & 57.7 \\ & 52.9 \end{aligned}$ | $\begin{aligned} & 90.6 \\ & 84.6 \\ & 78.5 \\ & 77.5 \\ & 6.5 .4 \end{aligned}$ | $\begin{array}{r} 114.3 \\ 106.7 \\ 99.1 \\ 91.4 \\ 83.8 \end{array}$ | $\begin{aligned} & 144.7 \\ & 135 . \\ & 125.4 \\ & 11.7 \\ & 106.1 \end{aligned}$ | $\begin{aligned} & 183.1 \\ & 170.9 \\ & 158.7 \\ & 146.5 \\ & 134.3 \\ & \hline \end{aligned}$ | 230.8 <br> 215.5 <br> 20.1 <br> 184.7 <br> 169.3 | $\begin{aligned} & 288.4 \\ & 286.4 \\ & 249.9 \\ & 243.9 \\ & 211.5 \end{aligned}$ | $\begin{aligned} & 370.4 \\ & 34.7 \\ & 321.7 \\ & 296.3 \\ & 271.6 \end{aligned}$ | $\begin{aligned} & \begin{array}{l} 468.8 \\ 437.5 \\ 406.3 \\ 375 \\ 375 \\ 343.8 \end{array}, ~ \end{aligned}$ | $\begin{aligned} & 578.7 \\ & 540.1 \\ & 501 . \\ & 463.6 \\ & 424.4 \end{aligned}$ | 732.4 <br> 683.6 <br> 634.8 <br> 585.9 <br> 537.1 | $\begin{aligned} & 1172 . \\ & 1094 . \\ & 1015 . \\ & 937.4 \\ & 859.3 \end{aligned}$ | 2341.2185.2029.1873.1717.1 | $\begin{aligned} & 4724 . \\ & 4 \\ & 409 . \\ & 4094 \\ & 3 \\ & 3 \\ & 3 \\ & 3 \end{aligned}$ | $\begin{aligned} & 7500 \\ & 7000 \\ & 7500 \\ & 65000 \\ & 6000 \\ & 5500 \end{aligned}$ | 69.4 <br> 64.8 <br> 60.1 <br> 55.5 <br> 50.9 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 500000450000400000350000300000 | $\begin{aligned} & 30.5 \\ & 37.5 \\ & 24.4 \\ & 21.4 \\ & 21.4 \end{aligned}$ | $\begin{aligned} & 48.1 \\ & 43.2 \\ & 38.4 \\ & 33.6 \\ & 28.8 \end{aligned}$ | $\begin{aligned} & \hline 60.4 \\ & 54.4 \\ & 48.3 \\ & 4.3 \\ & 36.2 \end{aligned}$ | $\begin{aligned} & 76.2 \\ & 66.6 \\ & 61.6 \\ & 63.3 \\ & \text { 45.7 } \end{aligned}$ | $\begin{aligned} & 96.5 \\ & \hline 6.8 \\ & 77.2 \\ & 67.5 \\ & 57.9 \end{aligned}$ | $\begin{array}{r} 122.1 \\ 109.8 \\ 97.6 \\ 8.4 \\ 73.4 \end{array}$ | $\begin{array}{r} 153.9 \\ 138.5 \\ 123.1 \\ 107.7 \\ 92.3 \end{array}$ | $\begin{array}{\|l\|l\|} 192.3 \\ 173.3 \\ 153.8 \\ 134.6 \\ 115.4 \end{array}$ | 246.922.21972172.8148.2 | $\begin{aligned} & 312.5 \\ & 281.3 \\ & 250.5 \\ & 218.8 \\ & 187.5 \end{aligned}$ | $\begin{aligned} & 385.8 \\ & 347.2 \\ & 308.6 \\ & 270.1 \\ & 271.5 \end{aligned}$ | $\begin{aligned} & 488.3 \\ & 439.5 \\ & 390.6 \\ & 341.8 \\ & 293.8 \end{aligned}$ | $\begin{aligned} & 781.1 \\ & 70.9 \\ & 624.9 \\ & 544.8 \\ & 468.7 \end{aligned}$ | $\begin{array}{\|c} 1561 . \\ 140 . \\ 124 . \\ 109 . \\ 1092.3 \\ 936.3 \end{array}$ | $\begin{aligned} & 3149 . \\ & 2883 . \\ & 2850 . \\ & 2520 . \\ & 2205 . \\ & 1890 \end{aligned}$ | 5000.4500.4000.35000.3000. | $\begin{aligned} & 46.3 \\ & 41.6 \\ & 37 . \\ & 32.4 \\ & 32.4 \end{aligned}$ |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 25000 | 15.3 24. |  | 30.2 | 38.1 | 48.2 | 61. | 77. | 96.1 | 123.5 | 156.3 | 192.9 | 244.2 | 390.6 | 780.3 | 1575. | 2500. | 23.1 |

NUMBERS OF WIRES IN STRANDS.-(Continued.)


## IRON WIRE.

IN COMPARING tables of the weights of Galvanized Iron Wire it was found that the weights of the various sizes were not consistent with each other in the same table, and that no two tables seemed to agree in regard to the specific gravity of the material.

This table is calculated from the formula, weight per mile $=\mathrm{D}^{2} \times .0139$, which seems to be the most likely value for galvanized iron wire. This corresponds with a specific gravity of 7.73 , and a weight per cubic foot of 483 pounds.

Steel wire is slightly heavier, and it is probable the constant in the above formula should be .014 for galvanized steel wire.

The following average values of the mile-ohm were used in calculating the resistance per mile at $68^{\circ} \mathrm{F}$., the International ohm being the unit:

| Kind of material. | Minimum. | Maximum. | Average. |
| :---: | :---: | :---: | :---: |
| E. B. B., | 4500 | 4800 | 4700 |
| B. B., | 5300 | 6000 | 5500 |
| Steel, | 6000 | 7000 | 6500 |

The breaking weight of any wire equals its weight per mile multiplied by 3 for E. B. B., 3.3 for B. B., or 3.7 for steel, all annealed and galvanized. This corresponds to 53100 pounds, 58410 pounds, and 65490 pounds per square inch, respectively.

The strength of steel wire varies from 50000 pounds per square inch to over 300000 pounds, according to the kind of material and its treatment.

By taking 100000 pounds per square inch as the breaking strain of steel wire, the breaking strain of any other wire may easily be computed from the table. For a wire of 80000 pounds per square inch breaking strain, take eight-tenths of the tabulated breaking strain for that size wire at 100000 pounds per square inch given in the table.

## GALVANIZED IRON WIRE.

|  |  | Weights. Pounds. |  | Breaking weights. Pounds. |  | Resistance per mile in ohms. |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & 1000 \\ & \text { feet. } \end{aligned}$ | One mile. | Iron. | Steel. | E. B. B. | B. B. | Steel. |
| 0 | 340 | 304 | 1607 | 4821 | 9079 | 2.93 | 3.42 | 4.05 |
| 1 | 300 | 237 | 1251 | 3753 | 7068 | 3.76 | 4.4 | 5.2 |
| 2 | 284 | 212 | 1121 | 3363 | 6335 | 4.19 | 4.91 | 5.8 |
| 3 | 259 | 177 | 932 | 2796 | 5268 | 5.04 | 5.9 | 6.97 |
| 4 | 238 | 149 | 787 | 2361 | 4449 | 5.97 | 6.99 | 8.26 |
| 5 | 220 | 127 | 673 | 2019 | 3801 | 6.99 | 8.18 | 9.66 |
| 6 | 203 | 109 | 573 | 1719 | 3237 | - 8.21 | 9.6 | 11.35 |
| 7 | 180 | 85 | 450 | 1350 | 2545 | 10.44 | 12.21 | 14.43 |
| 8 | 165 | 72 | 378 | 1134 | 2138 | 12.42 | 14.53 | 17.18 |
| 9 | 148 | 58 | 305 | 915 | 1720 | 15.44 | 18.06 | 21.35 |
| 10 | 134 | 47 | 250 | 750 | 1410 | 18.83 | 22.04 | 26.04 |
| 11 | 120 | 38 | 200 | 600 | 1131 | 23.48 | 27.48 | 32.47 |
| 12 | 109 | 31 | 165 | 495 | 933 | 28.46 | 33.3 | 39.36 |
| 13 | 95 | 24 | 125 | 375 | 709 | 37.47 | 43.85 | 51.82 |
| 14 | 83 | 18 | 96 | 288 | 541 | 49.08 | 57.44 | 67.88 |
| 15 | 72 | 13.7 | 72 | 216 | 407 | 65.23 | 76.33 | 90.21 |
| 16 | 65 | 11.1 | 59 | 177 | 332 | 80.03 | 93.66 | 110.7 |
| 17 | 58 | 8.9 | 47 | 141 | 264 | 100.5 | 120.4 | $139 .$ |
| 18 | 49 | 6.3 | 33 | 99 | 189 | 140.8 | 164.8 | 194.8 |

## GALVANIZED IRON TELEGRAPH WIRE.

Western Union Telegraph company's specifications. (Condensed).
" 1 . The wire to be soft and pliable, and capable of elongating 15 per cent. without breaking, after being galvanized.
" 2. Great tensile strength is not required, but the wire must not break under a less strain than two and onehalf times its weight in pounds per mile.
" 3 . Tests for ductility will be made as follows: The piece of wire will be gripped by two vises, 6 inches apart, and twisted. The full number of twists must be distinctly visible between the vises on the 6 -inch piece. The number of twists in a piece of 6 inches in length not to be under 15 .
" 4 . The weight per mile for the different gauge wires to be: for No. 4, 730 Ibs. ; No. 6, 540 Ibs.; No. 8, 380 Ibs.; No. $9,320 \mathrm{Hbs}$. No. ${ }^{10}, 250 \mathrm{Ibs}$., or, as near these figures as practicable.
" 5 . The electrical resistance of the wire in ohms per mile, at a temperature of $68^{\circ}$ Fahrenheit, must not exceed the quotient arising from the dividing the constant number 4800 by the weight of the wire in pounds per mile. The coëfficient .003 will be allowed for each degree Fahrenheit in reducing to standard temperature.
" 6 . The wire must be well galvanized, and capable of standing the following tests: The wire will be plunged into a saturated solution of sulphate of copper, and permitted to remain one minute, and then wiped clean. This process will be performed four times. If the wire appears black after the fourth immersion, it shows that the zinc has not been all removed, and that the galvanizing is well done ; but if it has a copper color, the iron is exposed, showing that the zinc is too thin."


## GALVANIZED SUPPORTING STRANDS.

What weight per foot will a half-inch ordinary strand support if the strain is one-half the breaking weight, the span 120 feet, and the deflection .01 of the span or 1.2 feet?

One-half the breaking weight of a half-inch ordinary galvanized strand is 4160 pounds. The value of S for above span and deflection, table page 50 , is 1500.2 . Dividing 4160 by 1500.2 we find the total weight per foot to be 2.773 pounds. Deducting from this the weight per foot of the half-inch galvanized strand we have 2.263 pounds as the weight per foot of cable that this strand will support. While it is true that a factor of safety of two in this work is too small, yet the cables help in a great measure to carry their own weight. It is believed that galvanized strands will easily carry the loads indicated on page 39.

This strand is composed of seven wires, twisted together into a single strand.

| Diameters in 32ds of an inch. | Weights per 100 feet. Pounds. | Estimated breaking strength. Pounds. |  |
| :---: | :---: | :---: | :---: |
|  |  | Ordinary. | Special. |
| 16 | 51 | 8320 | 16640 |
| 15 | 48 | 7500 | 15000 |
| 14 | 37 | 6000 | 12000 |
| 12 | 30 | 4700 | 9400 |
| 10 | 21 | 3300 | 6600 |
| 9 | 18 | 2600 | 5200 |
| 8 | 111/2 | 1750 | 3500 |
| 7 | $83 / 4$ | 1300 | 2600 |
| 6 | 61/2 | 1000 | 2000 |
| 5 | 41/2 | 700 | 1400 |
| 4 | 21/4 | 375 | 750 |
| 3 | 2 | 320 | 640 |


| JOHN |  |  | A. ROEBLING'S |  |  | SONS | CO. |  | 39 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SUPPORTING CAPACITY OF GALVANIZED STRANDS. <br> Ordinary. |  |  |  |  |  |  |  |  |  |
|  | Spans in feet. |  |  |  |  |  |  |  |  |
|  | 100 | 110 | 120 | 125 | 130 | 140 | 150 | 175 | 200 |
|  | Weights of 1000 feet of cable. Pounds. |  |  |  |  |  |  |  |  |
| 16 | 2818 | 2516 | 2263 | 2152 | 2050 | 1867 | 1709 | 1391 | 1154 |
| 15. | 2520 | 2247 | 2020 | 1920 | 1827 | 1663 | 1520 | 1234 | 1130 |
| 14 | 2030 | 1812 | 1630 | 1550 | 1476 | 1344 | 1230 | 1001 | 900 |
| 12 | 1580 | 1409 | 1266 | 1204 | 1146 | 1043 | 953 | 774 | 640 |
| 10 | 1110 | 899 | 890 | 846 | 805 | 733 | 670 | 544 | 450 |
| 9 | 860 | 765 | 680 | 652 | 620 | 563 | 513 | 414 | 340 |
| 8 | 585 433 | 521 <br> 385 | 468 846 | 445 329 | 423 | 385 | $\stackrel{352}{ }$ | 285 | 235 |
| 6 | ${ }_{337}$ | 381 300 | $\stackrel{340}{270}$ | $\stackrel{325}{ } 25$ | 245 | 223 | 204 | 165 | 172 |
| Spectal. |  |  |  |  |  |  |  |  |  |
|  | Spans in feet. |  |  |  |  |  |  |  |  |
|  | 100 | 110 | 120 | 125 | 130 | 140 | 150 | 175 | 200 |
|  | Weights of 1000 feet of cable. Pounds. |  |  |  |  |  |  |  |  |
| 16 | 6146 | 5482 | 5036 | 4814 | 4510 | 4244 | 3928 | 3292 | 2818 |
| 15 | 5520 | 4974 | 4520 | 4320 | 4134 | 3808 | 3520 | 2948 | 2520 |
| 12 | 4430 3460 | 3994 <br> 3118 | 3630 2832 | 3470 2708 | 3322 2592 2 | 3058 | 2830 | 2372 | 2030 |
| 10 | 2430 | 2008 | 1990 | 1 | 1820 | 1676 | 1550 | 1298 | 1580 1110 |
| 9876 |  |  |  |  | 1420 | 1306 | 1206 | 1008 | 860 |
|  | 1285 | 1157 | 1051 | 1005 | - 961 | -885 | 819 | 685 | 585 |
|  | 953 737 | 857 663 | 778 603 | 745 | 712 | 655 | 607 | 507 | 473 |
|  | 737 | 663 |  | 577 | 553 | 509 | 472 | 393 | 337 |
| Dip $=.01$ of span. <br> Factor of safety of two. |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |

## CURRENTS.

## FUSING EFFECTS OF CURRENTS.

Table giving the diameters of wires of various materials which will be fused by a current of given strength.
W. H. Preece, F.R.S.

$$
\mathrm{d}=\left(\frac{\mathrm{C}}{\mathrm{a}}\right)^{\frac{2}{3}}
$$

|  | Diameters in inches. |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{aligned} & \text { सं } \\ & \text { सें } \\ & 0.0 \\ & 0.0 \\ & 0 \text { On } \end{aligned}$ |  |  |  |  | ( |  |  |  |
|  | 0.0021 | 0.0026 | 0.0033 | 0.0033 | 0.0035 | 0.0047 | 0.0072 | 0.0083 | 0.00 |
| 2 | 0.0034 | 0.0041 | 0.0053 | 0.0053 | 0.0056 | 0.0074 | 0.0113 | 0.0132 | 0.012 |
| 3 | 0.0044 | 0.0054 | 0.007 | 0.0069 | 0.0074 | 0.0097 | -0.014 9 | 0.0173 | 0.016 |
| 4 | 0.0053 | 0.0065 | 0.0084 | 0.0084 | 0.0089 | 0.0117 | 0.0181 | 0.021 | 0.020 |
| 5 | 0.0062 | 0.0076 | 0.0098 | 0.0097 | 0.0104 | 0.0136 | 0.021 | 0.0243 | 0.023 |
| 10 | 0.0098 | 0.012 | 0.0155 | 0.015 | 0.0164 | 0.0216 | 0.0334 | . 0386 |  |
| 15 | 0.0129 | 0.0158 | 0.0203 | 0.0202 | 0.0215 | 0.0283 | 0.0437 | 0.0506 | 0.1 |
| 20 | 0.0156 | 0.0191 | 0.0246 | 0.0245 | 0.0261 | 0.0343 | 0.0529 | 0.0613 | 0.059 |
| 25 | 0.0181 | 0.0222 | 0.0286 | 0.0284 | 0.0303 | 0.0398 | 0.0614 | 0.0711 | 0.069 |
| 30 | 0.0205 | 0.025 | 0.0323 | 0.032 | 0.0342 | 0.045 | 0.0694 | 0.0803 | 0.0779 |
| 35 | 0.0227 | 0.0277 | 0.0358 | 0.035 | 0.0379 | 0.049 | 0.0769 | 0.089 |  |
| 40 | 0.0248 | 6. 0303 | 0.0391 | 0.0388 | 0.0414 | 0.0545 | 0.084 | 0.0973 | 0.094 |
| 45 | 0.0268 | 0.0328 | 0.0423 | 0.042 | 0.0448 | 0.0589 | 0.0909 | 0.1052 | 0.1021 |
| 50 | 0.0288 | 0.0352 | 0.0454 | 0.045 | 0.048 | 0.0632 | 0.0975 | 0.1129 | 0.1095 |
| 60 | 0.0325 | 0.0397 | 0.0513 | 0.0509 | 0.0542 | 0.0714 | 0.1101 | 0.1275 | 0.1237 |
| 70 | 0.036 | 0.044 | 0.0568 | 00564 | 0.0601 | 0.0791 | 0.122 | 0.1413 | 0.1371 |
| 80 | 0.0394 | 0.0481 | 0.0621 | 0.0616 | 0.0657 | 0.0864 | 0.1334 | 0.1544 | 0.1499 |
| 90 | 0.0426 | 0.052 | 0.6872 | 0.0667 | 0.0711 | 0.0935 | 0.1443 | 0.1671 | 0.1621 |
| 100 | 0.0457 | 0.0558 | 0.072 | 0.0715 | 0.0762 | 0.1003 | 0.1548 | 0.1792 | 0.1739 |
| 120 | 0.0516 | 0.063 | 0.0814 | 0.0808 | 0.0861 | 0.1133 | 0.1748 | 0.2024 | 0.1964 |
| 140 | 0.0572 | 0.0698 | 0.0902 | 0.0895 | 0.0954 | 0.1255 | 0.1937 | 0.2243 | 0.2176 |
| 160 | 0.0625 | 0.0763 | 0.0986 | 0.0978 | 0.1043 | 0.1372 | 0.2118 | 0.2452 | 0.2379 |
| 180 | 0.0676 | 0.0826 | 0.1066 | 0.1058 | 0.1128 | 0.1484 | 0.2291 | 0.2652 | 0.2573 |
| 200 | 0.0725 | 0.0856 | 0.1144 | 0.1135 | 0.121 | 0.1592 | 0.2457 | 0.2845 | 0.276 |
| 225 | 0.0784 | 0.0958 | 0.1237 | 0.1228 | 0.1309 | 0.1722 | 02658 | 0.3077 | 0.2986 |
| 250 | 0.0841 | 0.1028 | 0.1327 | 0.1317 | 0.1404 | 0.1848 | 0.2851 | 03301 | 0.3203 |
| 275 | 0.0897 | 0.1095 | 0.1414 | 0.1404 | 0.1497 | 0.1969 | 0.3038 | 0.3518 | 0.3417 |
| 300 | 0.095 | 0.1161 | 0.1498 | 0.1487 | 0.1586 | 0.2086 | 0.322 | 0.3728 | 0.3617 |

FUSING EFFECTS OF CURRENTS.-(Continued.)
Table showing the amperes required to fuse wires of various sizes and materials.

| ²0 | Diameter, d. | $\mathrm{d}^{\frac{3}{2}}$. | $\begin{aligned} & \text { Copper. } \\ & \mathrm{a}=10244 . \end{aligned}$ | $\underset{a=7585 .}{\text { Aluminum, }}$ | $\begin{aligned} & \text { Platinum, } \\ & \mathbf{a}=5172 . \end{aligned}$ | German silver, $a=5230$ | Platinoid, $a=4750$. | $\begin{gathered} \text { Iron, } \\ \mathrm{a}=3148 . \end{gathered}$ | $\underset{a=1642 .}{\operatorname{Tin},}$ | Tin-lead alloy, $a=1318$. | $\begin{gathered} \text { Lead, } \\ \mathrm{a}=1379 . \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 14 | 0.08 | 0.022627 | 231.8 | 171.6 | 117. | 118.3 | 107.5 | 71.22 | 37.15 | 29.82 | 31.2 |
| 16 | 0.064 | 0.016191 | 165.8 | 122.8 | 83.73 | 84.68 | 76.9 | 50.96 | 26.58 | 21.34 | 22.32 |
| 18 | 0.048 | 0.010516 | 107.7 | 79.75 | 54.37 | 54.99 | 49.95 | 33.1 | 17.27 | 13.86 | 14.5 |
| 20 | 0.036 | 0.006831 | 69.97 | 51.18 | 35.33 | 3572 | 32.44 | 21.5 | 11.22 | 9.002 | 9.419 |
| 22 | 0.028 | 0.004685 | 48. | 35.53 | 24.23 | 24.5 | 22.25 | 14.75 | 7.692 | 6.175 | 6.461 |
| 24 | 0.022 | 0.003263 | 33.43 | 24.75 | 16.88 | 17.06 | 15.5 | 10.27 | 5.357 | 4.3 | 4.499 |
| 26 | 0.018 | 0.002415 | 24.74 | 18.32 | 12.49 | 12.63 | 11.47 | 7.602 | 3.965 | 3.183 | 3.33 |
| 28 | 0.0148 | 0.001801 | 18.44 | 13.66 | 9.311 | 9.416 | 8.552 | 5.667 | 2.956 | 2.373 | 2.483 |
| 30 | 0.0124 | 0.001381 | 14.15 | 10.47 | 7.142 | 7.222 | 6.559 | 4.347 | 2.267 | 1.82 | 1.904 |
| 32 | 0.0108 | 0.001122 | 11.5 | 8.512 | 5.805 | 5.87 | 5.33 | 3.533 | 1.843 | 1.479 | 1.548 |

Note.-The size of "cut-outs," or fuses for electric-lighting circuits, can be taken at once from the first table. Pure copper wire makes the best and most reliable cut-out or fuse, and should never be less than one inch in length between the terminals to which it is fixed so as to prevent the cooling effect of the terminals.

## HEATING EFFECTS OF CURRENTS.

AREPORT read before the Edison Convention, at Niagara Falls, August, 1889, by A. E. Kennelly, gives complete formulæ and tables based on experimental data, showing the heating effects of electric currents. This report was published in the Electrical World, beginning with the edition of November 23, 1889.

The tables in this book are taken from curves constructed from data given in the above report.

The table page 43 gives the rules of the varions insurance companies, together with one column giving the current whose double would cause a rise of $40^{\circ} \mathrm{C}$. This is the safe carrying capacity recommended in Kennelly's report.

The table page 44 gives the diameters of various wires and the current they will carry with a specified rise in temperature. The wires are insulated, and the conditions are similar to those met with in house wiring in mouldings or conduits.

The table page 45 is computed for bare wires suspended indoors, and gives the current carried with the corresponding rise in temperature.

The table page 46 is computed for outdoor wires, not insulated.

In these tables all wires are solid.
Insulation increases the current a wire will carry with a given rise in temperature, because the radiating surface is increased, and for the same reason a strand will carry a larger current than a solid wire.

One square inch of bright copper radiates .0039 watts per degree Centigrade rise in temperature, and one square inch of blackened copper, .009 watts, under the same conditions. Convection seems to be dependent only on length, and may be taken at .053 watts per foot per degree Centigrade rise.

## HEATING EFFECTS OF CURRENTS.

Insurance rules for carrying capacity of wires.

|  |  |  | Nation of Fir wr Concealed work. | Board Underrs. $\qquad$ <br> Open work. | $\begin{aligned} & \text { Associated Factory } \\ & \text { Mutual Insurance } \\ & \text { company. } \end{aligned}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0000 | 174 | 175 | 218 | 312 | 175 | ..... |
| 000 | 146 | 145 | 181 | 262 | 145 | ..... |
| 00 | 123 | 120 | 150 | 220 | 120 | 105 |
| 0 | 103 | 100 | 125 | 185 | 100 | 83 |
| 1 | 88 | 95 | 105 | 156 | 85 | 66 |
| 2 | 73 | 70 | 88 | 131 | 70 | 52 |
| 3 | 61 | 60 | 75 | 110 | 60 | 41 |
| 4 | 52 | 50 | 63 | 92 | 50 | 33 |
| 5 | 43 | 45 | 53 | 77 | 45 | 26 |
| 6 | 36 | 35 | 45 | 65 | 35 | 21 |
| 7 | 31 | 30 | .... | .... | 30 | 16 |
| 8 | 26 | 25 | 33 | 46 | 25 | 13 |
| 10 | 18 | 20 | 25 | 32 | 20 | 8 |
| 12 | 18 | 15 | 17 | 23 | 15 | 5 |
| 14 | 9 | 10 | 12 | 16 | 10 | 3 |
| 16 | 6 | 5 | 6 | 8 | 5 | 2 |
| 18 | 5 | ..... | 3 | 5 | 3 | 1 |

## HEATING EPFECTS OF CURRENTS.-(Cont.)

Carrying capacity of insulated wires in mouldings.
(Kennelly's formula.)

|  | Rise in temperature in degrees Centigrade. |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $5^{\circ}$ | $10^{\circ}$ | $15^{\circ}$ | $20^{\circ}$ | $30^{\circ}$ | $40^{\circ}$ | $50^{\circ}$ | $60^{\circ}$ | $70^{\circ}$ |
|  | Diameters of wires in mils. |  |  |  |  |  |  |  |  |
| 300 | $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ | 446 | 411 | 386 | 367 | 354 |
| 280 | ..... | $\ldots$ |  |  | 427 | 393 | 369 | 350 | 338 |
| 260 | $\ldots$ | ..... | .... | 450 | 409 | 375 | 352 | 333 | 321 |
| 240 | ..... | ..... |  | 430 | 390 | 356 | 333 | 315 | 304 |
| 220 | ..... | ..... | 436 | 408 | 370 | 337 | 315 | 298 | 285 |
| 200 | $\ldots$ | 448 | 414 | 386 | 350 | 317 | 295 | 280 | 268 |
| 190 | ..... | 437 | 403 | 375 | 339 | 308 | 286 | 270 | 258 |
| 180 | ..... | 425 | 391 | 364 | 328 | 298 | 277 | 260 | 249 |
| 170 | ..... | 411 | 378 | 352 | 317 | 287 | 266 | 250 | 239 |
| 160 | ..... | 398 | 364 | 340 | 305 | 276 | 256 | 241 | 229 |
| 150 | 445 | 383 | 351 | 326 | 293 | 265 | 244 | 230 | 218 |
| 140 | 431 | 370 | 338 | 312 | 281 | 253 | 232 | 220 | 206 |
| 130 | 417 | 354 | 322 | 300 | 269 | 240 | 220 | 208 | 195 |
| 120 | 400 | 339 | 308 | 285 | 255 | 228 | 208 | 195 | 182 |
| 110 | 383 | 322 | 292 | 270 | 240 | 214 | 195 | 182 | 170 |
| 100 | 362 | 302 | 276 | 253 | 223 | 200 | 182 | 168 | 158 |
| 90 | 343 | 284 | 259 | 237 | 208 | 185 | 168 | 154 | 143 |
| 80 | 322 | 264 | 240 | 218 | 192 | 169 | 153 | 139 | 130 |
| 70 | 300 | 242 | 220 | 198 | 174 | 152 | 139 | 123 | 116 |
| 60 | 275 | 220 | 195 | 175 | 155 | 135 | 122 | 108 | 101 |
| 50 | 250 | 195 | 175 | 152 | 132 | 118 | 104 | 91 | 86 |
| 40 | 217 | 169 | 144 | 128 | 110 | 95 | 85 | 75 | 70 |
| 30 | 178 | 136 | 115 | 100 | 85 | 73 | 66 | 58 | 54 |
| 20 | 132 | 100 | 71 | 69 | 59 | 50 | 45 | 40 | 37 |
| 10 | 78 | 58 | 42 | 35 | 30 | $\cdots$ | ..... | ..... | ..... |

JOHN A．ROEBLING＇S SONS CO．

## HEATING EFFECTS OF CURRENTS．－（Cont．）

Bare copper in still air．
Rise in temperature，degrees Centigrade．

| $10^{\circ}$ |  | $20^{\circ}$ |  | $40^{\circ}$ |  | $80^{\circ}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { ざ } \\ & \text { 品 } \\ & \text { M } \end{aligned}$ |  | 咢 | 苍 | 呂 | － | 淢 | 烒 |

Diameters of wires in mils．


## HEATING EFFECTS OF CURRENTS．－（Cont．）

Bare copper suspended outdoors．

|  | Rise in temperature，degrees Centigrade． |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $5^{\circ}$ |  | $10^{\circ}$ |  | $20^{\circ}$ |  | $40^{\circ}$ |  |
|  | $\begin{aligned} & \text { 蔦 } \\ & \text { 感 } \end{aligned}$ | $\begin{aligned} & \text { ジせ } \\ & \text { 花 } \end{aligned}$ |  | 葛 | 号 | 萨 | 器 | 遍 |
|  | Diameters of wires in mils． |  |  |  |  |  |  |  |
| 1000 | ． | ．．．．． | 962 | 932 | 771 | 745 | 620 | 594 |
| 950 | ．．．．． | $\cdots$ | 9：8 | 897 | 744 | 720 | 595 | 572 |
| 900 | ．．．．． | ．．．．． | 894 | 865 | 715 | 692 | 574 | 552 |
| 850 | ．．．．． | ．．．．． | 868 | 843 | 689 | 665 | 550 | 530 |
| 800 | ．．．．． | ．．．．． | 839 | 810 | 672 | 649 | 537 | 512 |
| 750 |  | 975 | 804 | 775 | 643 | 6：0 | 515 | 495 |
| 700 | 963 | 933 | 767 | 739 | 613 | 591 | 491 | 472 |
| 650 | 916 | 889 | 729 | 703 | 582 | 561 | 467 | 449 |
| 600 | 869 | 837 | 690 | 665 | 554 | 532 | $44^{2}$ | 426 |
| 575 | 845 | 813 | 671 | 647 | 538 | 517 | 429 | 414 |
| 550 | 820 | 789 | 650 | 627 | 522 | 501 | 417 | 402 |
| 525 | 795 | 764 | 630 | 609 | 506 | 487 | 404 | 389 |
| 500 | 770 | 740 | 610 | 589 | 489 | 470 | 390 | 376 |
| 475 | 745. | 719 | 589 | 569 | 473 | 455 | 377 | 363 |
| 450 | 719 | 693 | 568 | 548 | 453 | 438 | 363 | 350 |
| 425 | 690 | 667 | 546 | 526 | 436 | 422 | 349 | 336 |
| 400 | 661 | 638 | 524 | 504 | 418 | 406 | 334 | 322 |
| 375 | 632 | 610 | 502 | 484 | 399 | 377 | 319 | 309 |
| 350 | 601 | 581 | 478 | 462 | 380 | 360 | 304 | 295 |
| 325 | 571 | 552 | 453 | 439 | 362 | 342 | 289 | 279 |
| 300 | 540 | 522 | 428 | 415 | 342 | 326 | 273 | 264 |
| 275 | 509 | 492 | 404 | 392 | 321 | 309 | 257 | 249 |
| 250 | 477 | 460 | 378 | 367 | 300 | 240 | 240 | 222 |
| 225 | 445 | 430 | 351 | 343 | 280 | 270 | 223 | 215 |
| 200 | 410 | 399 | 324 | 316 | 259 | 250 | 205 | 198 |
| 175 | 373 | 365 | 296 | 289 | 235 | 227 | 186 | 180 |
| 150 | 334 | 329 | 267 | 258 | 211 | 202 | 166 | 161 |
| 125 | 295 | 290 | 235 | 226 | 185 | 177 | 145 | 144 |
| 100 | 254 | 248 | 202 | 193 | 157 | 152 | 123 | 120 |
| 90 | 236 | 230 | 186 | 178 | 145 | 140 | 114 | 111 |
| 80 | 216 | 212 | 171 | 164 | 182 | 128 | 104 | 102 |
| 70 | 198 | 192 | 155 | 150 | 120 | 116 | 94 | 91 |
| 60 | 177 | $170^{\circ}$ | 137 | 132 | 107 | 104 | 83 | 80 |
| 50 | 155 | 147 | 119 | 115 | 92 | 87 | 72 | 70 |
| 40 | 130 | 124 | 100 | 96 | 77 | 73 | 62 | 59 |
| 30 | 104 | 100 | 78 | 75 | 61 | 58 | 50 | 45 |
| 20 | 73 40 | 70 | 54 | 53 | 43 | 40 | 34 | 30 |
| 10 | 40 | 38 | 27 | 26 | 20 | 18 | 16 | 14 |

## SPANS.

THE formulæ used in calculating these tables of lengths and strains in spans of wire are those of a catenary of small deflection. They are given in Weisbach's Mechanics of Engineering, page 297. (seventh American edition, translated by Eckley B. Coxe, A. M.)

In these tables the horizontal strain at the center of the span is given. The strain at any other point equals the strain at the center plus the weight of a length of the wire equal to the perpendicular distance of that point from the lowest point of the wire in the span. For ordinary spans this is negligible. For any given wire the longest possible span is one where the deflection is about one-third of the span.
The effects of temperature on the strains of wires in spans is at first sight so great as to render the other considerations of little importance. The table, page 53, is calculated on the assumption that the supports of the spans are perfectly rigid under all conditions of strain and that the wire is inelastic. This is never true in practice. The changes in direction in a pole line afford a chance for the strains, due to a shortening of the wire by a fall in temperature, to be taken up by a bending of the supports.

If the elastic limit of hard-drawn copper wire of 60000 pounds breaking strain be taken at 20000 pounds, then $S$ will equal 20000 divided by 3.85 , the weight of a piece of copper one foot long and one square inch in section. This makes $S$ equal 5195 . Looking at the table of values of S, page 50, this value for a span of 130 feet comes between a deflection of .003 and .004 . In the same way the allowable deflection fur any other span of hard-drawn copper could be found or for any other material by substituting the proper terms for the elastic limit and the weight per foot given above.

The following gives the practice of some of the telegraph and telephone companies in their line construction:

## SPECIFICATIONS FOR STANDARD CONSTRUCTION OF HARD-DRAWN COPPER.

|  | Spans in feet. |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 75 | 100 | ${ }^{\circ} 115$ | 130 | 150 | 200 |
|  | Sag in inches. |  |  |  |  |  |
| $-30$ | 1 | 2 | 21/2 | 38 | 41/2 | 8 |
| -10 | $11 / 2$ | $21 / 3$ | 3 | $3^{3 / 7}$ | 5 | ${ }^{9}$ |
| 10 | $11 / 3$ | $25 / 8$ | $31 / 2$ | 43 | $53 /$ | 101/4 |
|  |  |  |  |  |  |  |
| 60 80 | 21/2 | $41 / 1$ 59 | $51 / 2$ | 7 85 | ${ }_{111 / 4}$ | 153 18 |
| 100 |  | $7^{3 / 8}$ |  | $11^{8 / 8}$ |  | 1821/4 |

For spans between 400 and 600 feet, the dip shall be 1-40th of the span.

For spans between 600 and 1000 feet, the dip shall be 1-30th of the span.

Another company uses 40 poles to the mile, and in the East allows three-inch dip at center of spans. In the West, where the variation of temperature is greater, 10 inches dip is allowed in summer, and 8 inches in the winter. This construction applies to both copper and iron wire, and has been found by actual experience to give satisfactory results.

The following formulæ were used in calculating the tables:
(1) $\mathrm{S} \times \mathrm{W}=$ horizontal strain on wire at center of span
(2)

$$
\begin{align*}
& S=\frac{y^{2}}{2 x}+\frac{x}{6} \\
& 1=y\left[1+\frac{3}{3}\left(\frac{x}{y}\right)^{2}\right]  \tag{3}\\
& x=3 S-\sqrt{9 S^{2}-3 y^{3}}
\end{align*}
$$

(4)
(5)

$$
x=\sqrt{\frac{3 y l-3 y^{3}}{2}}
$$

## 249

JOHN A. ROEBLING'S SONS CO.

In these formula
$\mathrm{y}=$ one-half span.
$1=$ one-half length of wire in span.
$\mathrm{x}=$ deflection at center in same units as $y$.
$\mathrm{w}=$ weight per foot of wire.

Suppose we have a span of 200 feet of hard-drawn copper wire weighing one pound to 10 feet, and a deflection of two feet or .01 of the span.

$$
\begin{align*}
S & =\left(\frac{100}{2}\right)^{2}+\frac{2}{6}  \tag{2}\\
& =2500.33+
\end{align*}
$$

$$
\begin{align*}
1 & =100\left[1+\frac{3}{3}\left(\frac{2}{100}\right)^{2}\right]  \tag{3}\\
& =100.0266+ \\
21 & =200.053+
\end{align*}
$$

$$
\begin{align*}
\mathrm{x} & =7501-\sqrt{56265001-30000 .}  \tag{4}\\
& =2
\end{align*}
$$

$$
\begin{align*}
\mathbf{x} & =\sqrt{\frac{30008-30000}{2 .}}  \tag{5}\\
& =2 .
\end{align*}
$$

In calculating the table, page 53, the deflection of the line was determined at $-10^{\circ} \mathrm{F}$. by formula 4 , the value of $S$ being 30000 divided by 3.85 or 7792 . For the other temperatures the length of the wire was calculated from the following formula:

$$
\text { Length }=1(1+.0000093 t)
$$

Here t is the difference in temperature in degrees Fahrenheit.

By formula 5 the deflection corresponding to the new length was found.

The coëfficients of linear expansion for each degree Fahrenheit are as follows:

> | Copper, .0000093. |
| :--- |
| Iron, |
| Lead, .0000068. |
| 000016. |

STRAINS AT CENTERS OF SPANS RESULTING FROM A GIVEN DEFLECTION.-(Cont.)

|  | Deflectlons in decimal parts of spans. |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | . 020 | . 025 | 030 | . 035 | . 040 | . 045 | . 050 | . 055 | . 060 | . 065 | . 070 | . 075 |
|  | Multipliers. |  |  |  |  |  |  |  |  |  |  |  |
| 10 | 62.533 | 50.041 | 41.716 | 35.772 | 31.316 | 27.852 | 25.083 | 22.818 | 20.933 | 19.339 | 17.973 |  |
| 20 | 125.066 | 100.083 | 83.433 | 71.545 | 62.633 | 55.705 | 50.166 | 45.637 | 41.866 | 38.678 | 35.947 | ${ }_{33.583}$ |
| 30 | 187.6 | 150.125 | 125.15 | 107.317 | 93.950 | 83.558 | 75.25 | 68.456 | 62.8 | 58017 | 53.921 | 50.375 |
| 40 | 250.133 | 200.166 | 166.866 | 143.09 | 125.266 | 111.411 | 100.333 | 91.275 | 83.733 | 77.356 | 71.895 | 67.166 |
| 50 | 312.666 | 250.208 | 208.583 | 178.863 | 156.583 | 139.263 | 125.416 | 114.094 | 104.666 | 96.695 | 89.869 | 83.958 |
| 60 | 375.2 | 300.25 | 250.3 | 214.635 | 187.900 | 167.116 | 150.5 | 136.913 | 125.6 | 116.034 | 107.042 | 100.75 |
| 70 | 437.733 | 350.291 | 292.016 | 250.408 | 219.216 | 194.969 | 175.583 | 159.732 | 146.533 | 135.373 | 125.816 | 117.541 |
| 80 | 500.266 | 400.333 | 333.733 | 286.18 | 250.533 | 222.822 | 200.666 | 182.551 | 167.466 | 154.712 | 143.79 | 134.333 |
| 90 | 562.8 | 450.375 | 375.45 | 321.953 | 281.850 | 250.674 | 225.75 | 205.37 | 188.4 | 174.051 | 161.764 | 151.125 |
| 100 | 625333 | 500.416 | 417.166 | 357.726 | 313.166 | 278.527 | 250.833 | 228.189 | 209.333 | 193.391 | 179.738 | 167.916 |
| 110 | 687.866 | 550.458 | 458.883 | 393.498 | 344.483 | 306.38 | 275.916 | 251.008 | 230.266 | 212.73 | 197.711 |  |
| 120 | 750.4 | 600.5 | 500.6 | 429.271 | 375.800 | 334.233 | 301. | 273.827 | 251.2 | 232.069 | 215.685 | 201.5 |
| 130 | 812.933 | 650.541 | 542.316 | 465.044 | 407.116 | 362.086 | 326.083 | 296.646 | 272.133 | 251.408 | 233.659 | 218.291 |
| 140 | 875.466 | 700.583 | 584.033 | 500.816 | 438.433 | 389.938 | 351.166 | 319.465 | 293.066 | 270.747 | 251.633 | 235.083 |
| 150 | 938. | 750.625 | 625.75 | 536.589 | 469.750 | 417.791 | 376.25 | 342.284 | 314. | 290.086 | 269.607 | 251.875 |
| 160 | 1000.533 | 800.666 | 667.466 | 572.361 | 501.066 |  | 401.333 | 365.103 | 334.933 | 309.425 | 287.58 | 268.666 |
| 170 | 1063.066 | 850.708 | 709.183 | 608.134 | 532.383 | 473.497 | 426.416 | 387.921 | 355.866 | 328.764 | 305.554 | 285.458 |
| 180 | 1125.6 | 900.75 | 750.9 | 643.907 | 563.7 | 501.349 | 451.5 | 410.74 | 376.8 | 348.103 | 323.528 | 302.25 |
| 190 | 1188.133 | 950.791 | 792.616 | 679.679 | 595.016 | 529.202 | 476.583 | 433.559 | 397.733 | 367.442 | 341.502 | 319.041 |
| 200 | 1250.666 | 1000.833 | 834.333 | 715.452 | 626.333 | 557.055 | 501.666 | 456.378 | 418.666 | 386.782 | ${ }_{359.476}$ | ${ }_{335.833}$ |

STRAINS AT CENTERS OF SPANS RESULTING FROM A GIVEN DEFLECTION.-(Cont.)

|  | Deflections in decimal parts of spans. |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | . 080 | . 085 | . 090 | . 095 | . 100 | . 110 | . 120 | . 130 | . 140 | . 150 | . 160 | . 170 | . 180 | . 190 | . 200 |
|  | Multipliers. |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | 15.758 | 14.847 | 14.038 | 13.316 | 12.666 | 11.546 | 10.616 | 9.832 | 9.161 | 8.583 | 8.079 | 7.636 | 7.244 | 6.895 | 6.583 |
| 20 | 31.516 | 29.695 | 28.077 | 26.632 | 25.333 | 23.093 | 21.233 | 19.664 | 18.323 | 17.166 | 16.158 | 15.272 | 14.488 | 13.791 | 13.166 |
| 30 | 47.275 | 44.542 | 42.116 | 39.948 | 38. | 34.64 | 31.85 | 29.496 | 27.485 | 25.75 | 24.237 | 22.908 | 21.733 | 20.686 | 19.75 |
| 40 | 63.033 | 59.39 | 56.155 | 53.264 | 50.666 | 46.187 | 42.466 | 39.328 | 36.647 | 34.333 | 32.316 | 30.545 | 28.977 | 27.582 | 26.333 |
| 50 | 78.791 | 74.237 | 70.194 | 66.581 | 63.333 | 57.734 | 53.083 | 49.16 | 45.809 | 42.916 | 40.395 | 38.181 | 36.222 | 34.478 | 32.916 |
| 60 | 94.55 | 89.085 | 84.233 | 79.897 | 76. | 69.281 | 63.7 | 58.992 | 54.971 | 51.5 | 48.475 | 45.817 | 43.466 | 41.373 | 39.5 |
| 70 | 110.308 | 103.932 | 98.272 | 93.213 | 88.666 | 80.828 | 74.316 | 68.824 | 64.133 | 60.083 | 56.554 | 53.453 | 50.711 | 48.269 | 46.083 |
| 80 | 126.066 | 118.78 | 112.311 | 106.529 | 101.333 | 92.375 | 84.933 | 78.656 | 73.295 | 68.666 | 64.633 | 61.09 | 57.955 | 55.164 | 52.666 |
| 90 | 141.825 | 133.627 | 126.35 | 119.846 | 114. | 103.922 | 95.55 | 88.488 | 82.457 | 77.25 | 72.712 | 68.726 | 65.199 | 62.06 | 59.25 |
| 100 | 157.583 | 148.475 | 140.388 | 133.162 | 126.666 | 115.469 | 106.166 | 98.32 | 91.619 | 85.833 | 80.791 | 76.362 | 72.444 | 68.956 | 65.833 |
| 110 | 173.341 | 163.323 | 154.427 | 146.478 | 139.333 | 127.016 | 116.783 | 108.152 | 100.78 | 94.416 | 88.87 | 83.999 | 79.688 | 75.851 | 72.416 |
| 120 | 189.1 | 178.17 | 168.466 | 159.794 | 152. | 138.563 | 127.4 | 117.984 | 109.942 | 103. | 96.95 | 91.635 | 86.933 | 82.747 | 79. |
| 130 | 204.858 | 193.018 | 182.505 | 173.11 | 164.666 | 150.11 | 138.016 | 127.816 | 119.104 | 111.583 | 105.029 | 99.271 | 94.177 | 89.642 | 85.583 |
| 140 | 220.616 | 207.865 | 196.544 | 186.427 | 177.333 | 161.657 | 148.633 | 137.648 | 128.266 | 120.166 | 113.108 | 106.907 | 101.422 | 96.538 | 92.166 |
| 150 | 236.375 | 222.713 | 210.583 | 199.743 | 190. | 173.204 | 159.25 | 147.48 | 137.428 | 128.75 | 121.187 | 114.544 | 108.666 | 103.434 | 98.75 |
| 160 | 252.133 | 237.56 | 224.622 | 213.059 | 202.666 | 184.751 | 169.866 | 157.312 | 146.59 | 137.333 | 129.266 | 122.18 | 115.911 | 110.329 | 105.333 |
| 170 | 267.891 | 252.408 | 238.661 | 226.375 | 215.333 | 196.298 | 180.483 | 167.144 | 155.752 | 145.916 | 137.345 | 129.816 | 123.155 | 117.225 | 111.916 |
| 180 | 283.65 | 267.255 | 252.7 | $239.69{ }^{2}$ | 228. | 207.845 | 191.1 | 176.976 | 164.914 | 154.5 | 145.425 | 137.452 | 130.399 | 124.121 | 118.5 |
| 190 | 299.408 | 282.103 | 266.738 | 253.008 | 240.666 | 219.392 | 201.716 | 186.808 | 174.076 | 163.083 | 153.504 | 145.089 | 137.644 | 131.016 | 125.083 |
| 200 | 315.166 | 296.95 | 280.777 | 266.324 | 253.333 | 230.939 | 212.333 | 196.641 | 183.238 | 171.666 | 161.583 | 152.725 | 144.884 | 137.912 | 131.666 |

[^3]
## TEMPERATURE EFFECTS IN SPANS.

| Spans in feet. | Temperature in degrees Fahrenheit. |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $-10^{\circ}$ | $30^{\circ}$ | $40^{\circ}$ | $50^{\circ}$ | $60^{\circ}$ | $70^{\circ}$ | $80^{\circ}$ | $90^{\circ}$ | $100^{\circ}$ |
|  | Deflections in inches. |  |  |  |  |  |  |  |  |
| 50 | . 5 | 6 | 8 | 9 | 9 | 10 | 11 | 11 | 12 |
| 60 | . 7 | 8 | 10 | 11 | 11 | 12 | 13 | 13 | 14 |
| 70 | 1. | 10 | 11 | 12 | 13 | 14 | 15 | 15 | 17 |
| 80 | 1.2 | 11 | 13 | 14 | 15 | 16 | 17 | 18 | 19 |
| 90 | 1.6 | 13 | 14 | 16 | 17 | 18 | 19 | 20 | 21 |
| 100 | 1.9 | 14 | 16 | 17 | 19 | 20 | 21 | 23 | 24 |
| 110 | 2.3 | 16 | 18 | 19 | 21 | 22 | 24 | 25 | 26 |
| 120 | 2.8 | 17 | 19 | 21 | 22 | 24 | 26 | 27 | 28 |
| 130 | 3.2 | 19 | 21 | 23 | 25 | 26 | 28 | 29 | 31 |
| 140 | 3.7 | 20 | 23 | 25 | 27 | 28 | 30 | 32 | 33 |
| 110 | 4.3 | 22 | 24 | 26 | 28 | 30 | 32 | 34 | 36 |
| 160 | 4.9 | 23 | 26 | 28 | 30 | 32 | 34 | 36 | 38 |
| 170 | 5.5 | 25 | 28 | 30 | 32 | 35 | 37 | 38 | 40 |
| 180 | 6.2 | 26 | 29 | 32 | 34 | 37 | 39 | 41 | 43 |
| 190 | 7. | 28 | 31 | 34 | 36 | 39 | 41 | 43 | 45 |
| 200 | 7.7 | 31 | 33 | 36 | 38 | 41 | 43 | 45 | 48 |

Hard-drawn copper wire, 60000 pounds strength per square inch.

Strain at $-10^{\circ} \mathrm{F}$., 30000 pounds per square inch.
TOTAL LENGTHS OF WIRES IN SPANS.-(Continued.)

|  | Deflections in decimal parts of spans. |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | . 090 | . 100 | . 110 | . 120 | . 130 | . 140 | . 150 | . 160 | . 170 | . 180 | . 190 | . 200 |
|  | Lengths of wires. |  |  |  |  |  |  |  |  |  |  |  |
| 10 | 10.216 | 10.266 | 10.322 | 10.384 | 10.45 | 10.522 | 10.6 | 10.682 | 10.77 | 10.864 | 10.962 | 11.066 |
| 20 | 20.432 | 20.533 | 20.645 | 20.768 | 20.901 | 21.045 | 21.2 | 21.365 | 21.541 | 21.728 | 21.925 | 22.133 |
| 30 | 30.648 | 30.8 | 30.968 | 81.152 | 31.352 | 31.568 | 31.8 | 32.048 | 32.312 | 32.592 | 32.888 | 33.2 |
| 40 | 40.864 | 41.066 | 41.29 | 41.536 | 41.802 | 42.09 | 42.4 | 42.73 | 43.082 | 43.456 | 43.85 | 44.266 |
| 50 | 51.08 | 51.333 | 51.613 | 51.92 | 52.253 | 52.613 | 53. | 53.413 | 53.853 | 54.32 | 54.813 | 55.333 |
| 60 | 61.296 | 61.6 | 61.936 | 62.304 | 62.704 | 63.136 | 63.6 | 64.096 | 64624 | 65.184 | 65.776 | 66.4 |
| 70 | 71.512 | 71.866 | 72.258 | 72.688 | 73.154 | 73.658 | 74.2 | 74.778 | 75.394 | 76.048 | 76.738 | 77.466 |
| 80 | 81.728 | 82.133 | 82.581 | 83.072 | 83.605 | 84.181 | 84.8 | 85.461 | 86.165 | 86.912 | 87.701 | 88.533 |
| 90 | 91.944 | 92.4 | 92.904 | 93.456 | 94.056 | 94.704 | 95.4 | 96.144 | 96.936 | 97.776 | 98.664 | 99.6 |
| 100 | 102.16 | 102.666 | 103.226 | 103.84 | 104.506 | 105.226 | 106. | 106.826 | 107.706 | 108.64 | 109626 | 110.666 |
| 110 | 112.376 | 112.933 | 113.549 | 114.224 | 114.957 | 115.749 | 116.6 | 117.509 | 118.477 | 119.504 | 120.589 | 121.733 |
| 120 | 122.592 | 123.2 | 123872 | 124.608 | 125.408 | 126.272 | 127.2 | 128.192 | 129.248 | 130.368 | 131.552 | 132.8 |
| 130 | 132.808 | 133.466 | 134.194 | 134.992 | 135.858 | 136.794 | 137.8 | 138.874 | 140.018 | 141.232 | 142.514 | 143.866 |
| 140 | 143.024 | 143.733 | 144.517 | 145.376 | 146.309 | 147.317 | 148.4 | 149.557 | 150.789 | 152.096 | 153.477 | 154.933 |
| 150 | 153.24 | 154. | 154.84 | 155.76 | 156.76 | 157.84 | 159. | 160.24 | 161.56 | 162.96 | 164.44 | 166. |
| 160 | 163.456 | 164.266 | 165.162 | 166.144 | 167.21 | 168.362 | 169.6 | 170.922 | 172.33 | 173.824 | 175.402 | 177.066 |
| 170 | 173.672 | 174.533 | 175.485 | 176.528 | 177.661 | 178.885 | 180.2 | 181.605 | 183.101 | 184.688 | 186.365 | 188.133 |
| 180 | 183.888 | 184.8 | 185.808 | 186.912 | 188.112 | 189.408 | 190.8 | 192.288 | 193.872 | 195.552 | 197.328 | 199.2 |
| 190 | 194.104 | 195.066 | 196.13 | 197.296 | 198.562 | 199.93 | 201.4 | 202.97 | 204.642 | 206.416 | 208.29 | 210.166 |
| 200 | 204.32 | 205.333 | 206.453 | 207.68 | 209.013 | 210.453 | 212. | 213.653 | 215.413 | 217.28 | 219.253 | 221.333 |

## WEATHERPROOF WIRE.

Our Weatherproof wire is put on reels in long lengths, and has a hard, smooth finish, presenting the least posisible chance fnr adherence of ice and snow. We keep in stock all sizes given in the accompanying table, to 0000 B. \& S., in both double and triple braid.

In the Stranded wires, we keep only the most commonly used sizes. We make this Feed Wire Strand either concentric or cable-laid, as desired.

## FIRE AND WEATHERPROOF WIRE.

For interior work, we manufacture a Fire and Weatherproof insulation. Full information concerning weights, diameters and prices furnished on application.

## UNDERWRITERS' WIRE.

Underwriters' wire seems to be used chiefly for inside work. Its weight is about the same as double-braid Weatherproof.

## WEATHERPROOF IRON WIRE.

We keep in stock 10,12 and 14 B. W. G., both double and triple braid.

| Numbers, B. W. G. | Weights per mile. Pounds. |  | Lengths in coils. Miles. |
| :---: | :---: | :---: | :---: |
|  | Double braid. | Triple braid. |  |
| 4 | 997 | 1102 |  |
| 6 | 713 | 773 | 1/8 |
| 8 | 483 | 548 | $1 / 4$ |
| 9 | 403 | 464 | 1/8 |
| 10 | 350 | 410 | 1/8 |
| 12 | 240 | 265 | 1/2 |
| 14 | 150 | 176 | 1/2 |

## WEATHERPROOF WIRE.

|  | Double braid. |  |  | Triple braid. |  |  | Approximate weights. Pounds. |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Weights. Pounds. |  |  | Weights. Pounds. |  |  |  |
|  |  | $\begin{aligned} & 1000 \\ & \text { feet. } \end{aligned}$ | Mile. |  | $\begin{aligned} & 1000 \\ & \text { feet. } \end{aligned}$ | Mile. | Reel. | Coil. |
| 0000 | 20 | 716 | 3781 | 24 | 775 | 4092 | 2000 | 250 |
| 000 | 18 | 575 | 3036 | 22 | 630 | 3326 | 2000 | 250 |
| 00 | 17 | 465 | 2455 | 18 | 490 | 2587 | 500 | 250 |
| 0 | 16 | 375 | 1980 | 17. | 400 | 2112 | 500 | 250 |
| 1 | 15 | 285 | 1505 | 16 | 306 | 1616 | 500 | 250 |
| 2 | 14 | 245 | 1294 | 15 | 268 | 1415 | 500 | 250 |
| 3 | 13 | 190 | 1003 | 14 | 210 | 1109 | 500 | 250 |
| 4 | 11 | 152 | 803 | 12 | 164 | 866 | 250 | 125 |
| 5 | 10 | 120 | 634 | 11 | 145 | 766 | 260 | 130 |
| 6 | 9 | 98 | 518 | 10 | 112 | 591 | 275 | 140 |
| 8 | 8 | 66 | 349 | 9 | 78 | 412 | 200 | 100 |
| 10 | 7 | 45 | 238 | 8 | 55 | 290 | 200 | 100 |
| 12 | 6 | 30 | 158 | 7 | 35 | 185 | ..... | 25 |
| 14 | 5 | 20 | 106 | 6 | ${ }^{26}$ | 137 | ..... | 25 |
| 16 | - 4 | 14 | 74 | 5 | 20 | 106 | $\ldots$ | 25 |
| 18 | 3 | 10 | 53 | 4 | 16 | 85 | ..... | 25 |

## STRANDED WEATHERPROOF FEED WIRE.

| Circular mils. | Outside diameters. lnches. | Weights. Pounds. |  | $\begin{gathered} \text { Approxi- } \\ \text { mate } \\ \text { length } \\ \text { on reels. } \\ \text { Feet. } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: |
|  |  | 1000 feet. | Mile. |  |
| 1000000 | 11/2 | 3550 | 18744 | 800 |
| 900000 | $11{ }^{1}$ | 3215 | 16975 | 800 |
| 800000 | $1{ }^{18}$ | 2880 | 15206 | 850 |
| 750000 | 15 | 2713 | 14325 | 850 |
| 700000 | $1{ }^{18}$ | 2545 | 13438 | 900 |
| 650000 | $11 / 4$ | 2378 | 12556 | 400 |
| 600000 | $1{ }^{3}$ | 2210 | 11668 | 1000 |
| 550000 | $1{ }^{1 / 8}$ | 2043 | 10787 | 1200 |
| 500000 | $11 / 8$ | 1875 | 9900 | 1320 |
| 450000 | $1{ }^{\frac{3}{31}}$ | 1703 | 8992 | 1400 |
| 400000 | $1{ }^{18}$ | 1530 | 8078 | 1450 |
| 350000 | 1 | 1358 | 7170 | 1500 |
| 300000 | $\frac{18}{18}$ | 1185 | 6257 | 1600 |
| 250000 | ${ }^{3}$ 景 | 1012 | 5343 | 1600 |

The table is calculated for concentric strands. Rope-laid strands are larger.

## RUBBER WIRE.

WE MANUFACTURE rubber insulated wires for all purposes, including wires and cables for aerial, underground, and submarine use. The copper conductor is tinned, and then covered with a cement of pure rubber, which causes the succeeding coat of rubber to adhere firmly to the wire. This layer consists of white rubber without sulphur. Over this is a layer of vulcanized rubber, and the whole is covered with a finishing braid of cotton saturated with a Weatherproof compound, which protects the rubber from mechanical injury, and from the action of the air. A poor quality of rubber insulation is inferior to Weatherproof, and we would recommend our Fire and Weatherproof insulation for inside work, rather than an inferior rubber wire.

A good rubber wire should have its conductor central, the insulation should adhere firmly to the wire, it should not crack or become brittle after use, and it should show, after immersion in water for twenty-four hours, the same insulation resistance per mile as when tested after being first put in water. The absolute number of megohms per mile depends on the age of the rubber used, together with other details of manufacture, and is not always a sure guide to the quality of the insulation. Uniformity of insulation among several coils of wire made at the same time, or among the various conductors of a cable, is a much more valuable aid in detecting a poor piece of wire, as in this case an insulation lower than the average shows a local defect, which, in time, will be likely to cause trouble.

## CRESCENT RUBBER WIRE

Stranded conductors.

| Numbers, <br> B. \& S. G. | $\begin{aligned} & \text { Circular } \\ & \text { mils. } \end{aligned}$ | Outside diameters. Inches. | Weights per 1000 feet. Pounds. | Sizes of wires in strands. B. \& S. G. |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Regular. | Flexible. |
| ........ | 1000000 | $1{ }_{18}^{78}$ | 3690 | 8 | 12 |
| ........ | 900000 | 113 | 3370 | 8 | 12 |
| ....... | 800000 | $1{ }^{92}$ | 3020 | 8 | 12 |
| ....... | 700000 | $1 \frac{7}{32}$ | 2685 | 10 | 12 |
| .... | 600000 | $1{ }_{37}{ }^{\frac{8}{3}}$ | 2345 | 10 | 12 |
| $\ldots$ | 500000 | 18 | 1885 | 10 | 14 |
| ... | 450000 | $1 \frac{18}{12}$ | 1723 | 10 | 14 |
| ....... | 400000 | 1 | 1560 | 10 | 14 |
| ........ | 350000 | $\frac{15}{18}$ | 1378 | 10 | 14 |
| ........ | 300000 | 7/8 | 1155 | 10 | 14 |
|  | 250000 | ${ }^{27}$ | 995 | 10 | 14 |
| 0000 | ......... | ${ }^{23}$ | 866 | 10 | 15 |
| 000 | ......... | ${ }^{2} \frac{3}{2}$ | 725 | 10 | 15 |
| 00 | ......... | 12 | 613 | 11 | 15 |


|  | Outside diameters in 32ds of an inch. |  | Weights per 1000 feet. Pounds. | Sizes of wires in strand. B. \& S. G. |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Solid. | Stranded. |  | Regular. | Flexible. |
| 0 | 18 | 20 | 489 | 12 | 16 |
| 1 | 16 | 18 | 393 | 12 | 16 |
| 2 | 14 | 15 | 309 | 12 | 18 |
| 3 | 13 | 14 | 244 | 13 | 18 |
| 4 | 12 | 13 | 198 | 14 | 20 |
| 5 | 11 | 12 | 168 | 15 | 20 |
| 6 | 10 | 11 | 146 | 16 | 20 |
| 8 |  | 10 | 106 | 18 | 22 |
| 10 | 8 | 8 | 77 | 20 | 25 |
| 12 | 7 | 7 | 55 | 20 | 25 |
| 14 | 6 | 6 | 35 | 21 | 25 |
| 16 | 5 | 5 | 25 | 23 | 25 |
| 18 | 4 | 4 | 20 | 25 | 25 |

## MAGNET WIRE.

THE BARE COPPER intended for Magnet wire is specially drawn and annealed, great care being taken to have it true to gauge, and soft.

A difference from the standard, of one mil, is allowed on sizes larger than No. 10 B. \& S. G.; from No. 10 to No. 14, three-fourths of a mil variation is allowed, and any wire smaller than No. 14, one-half a mil variation is allowed.

The insulation is smooth and uniform, and is kept true to gauge to within one mil of the required diameter.

We manufacture any special kind of Magnet wire required, flats, squares and strands.

We understand that a No. 6 B. \& S. square Magnet wire measures $162 \times 162$ mils.

Flats are designated by their width and thickness. Thus a flat Magnet wire 340 mils wide and 40 mils thick would be designated as a $340 \times 40$ flat Magnet wire.
Strands can be furnished of any size, insulated with double or triple windings of cotton, or any combination of braids and windings that may be desired.

## MAGNET WIRE.

| Numbers, <br> B. \& S. G. | $\begin{aligned} & \text { Diameter } \\ & \text { drawn. } \\ & \text { Mils. } \end{aligned}$ | Outside diameters. Mils. |  | Approximate weights on reels. Pounds. |
| :---: | :---: | :---: | :---: | :---: |
|  |  | Double. | Single. |  |
| 0 | 325 | 343 | 337 | 200 |
| 1 | 289 | 307 | 301 | 200 |
| 2 | 258 | 276 | 270 | 200 |
| 8 | 229 | 247 | 241 | 200 |
| 4 | 204 | 222 | 216 | 200 |
| 5 | 182 | 200 | 194 | 200 |
| 6 | 162 | 178 | 172 | 200 |
| 7 | 144 | 160 | 154 | 200 |
| 8 | 128 | 142 | 137 | 200 |
| 9 | 114 | 126 | 122 | 200 |
| 10 | 102 | 112 | 108 | 200 |
| 11 | 91 | 101 | 97 | 200 |
| 12 | 81 | 91 | 87 | 200 |
| 13 | 72 | 81 | 78 | 160 |
| 14 | 64 | 73 | 70 | 160 |
| 15 | 57 | 66 | 63 | 50 |
| 16 | 51 | 60 | 57 | 50 |
| 17 | 45 | 54 | 51 | 50 |
| 18 | 40 | 49 | 46 | 50 |
| 19 | 36 | 45 | 42 | 50 |

## GERMAN SILVER WIRE.

|  | Resistance perfeet. |  |  | Resistance per 1000 feet. |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 18 per centum. | 30 per centum. |  | 18 per centum. | 30 per centum. |
| 6 | 7.20 | 11.21 | 22 | 295.38 | 459.48 |
| 7 | 9.12 | 14.18 | 23 | 370.26 | 575.96 |
| 8 | 11.54 | 17.95 | 24 | 468.18 | 728.28 |
| 9 | 14.55 | 22.63 | 25 | 590.22 | 918.12 |
| 10 | 18.18 | 28.28 | 26 | 748.08 | 1163.68 |
| 11 | 22.84 | 35.53 | 27 | 937.98 | 1459.08 |
| 12 | 28.81 | 44.82 | 28 | 1191.24 | 1853.04 |
| 13 | 36.48 | 56.75 | 29 | 1481.22 | 2304.12 |
| 14 | 46.17 | 71.82 | 30 | 1891.8 | 2942.8 |
| 15 | 58.21 | 90.55 | 31 | 2388.6 | 3715.6 |
| 16 | 72.72 | 113.12 | 32 | 2955.6 | 4597.6 |
| 17 | 93.40 | 145.29 | 33 | 3751.2 | 5835.2 |
| 18 | 118.20 | 183.87 | 34 | 4764.6 | 7411.6 |
| 19 | 145.94 | 227.02 | 35 | 6031.8 | 9382.8 |
| 20 | 184.68 | 287.28 | 36 | 7565.4 | 11768.4 |
| 21 | 232.92 | 362.32 | ... | ......... | .......... |

The resistance of German silver wire varies according to the method of manufacture and the materials used.

From actual tests on wire with eighteen per centum of nickel, extending over ten years, it seems that eighteen times the resistance of copper, at $75^{\circ} \mathrm{F}$., represents very closely the resistance of this alloy. This value is rather under than over the average results of the tests.

For the thirty per centum alloy, we have to depend on the results of a single series of tests, and while the results are believed to be correct, they are not as reliable as those given for the eighteen per centum German silver wire. We take the resistance of the thirty per centum alloy at twenty-eight times the resistance of copper, at $75^{\circ}$.

The International ohm is taken as the unit of resistance.

## OFFICE WIRES.

Office wire is usually made with a wind and a braid of cotton saturated with paraffine. It is sometimes required with a double braid or triple braid of cotton. The most common colors are red and white. Any combination of colors can be furnished.
Damp-proof Office wire has the inside wind saturated with black Weatherproof compound, while the outside finish is the same as ordinary Office wire.

Annunciator wire has a covering consisting of two wraps of cotton saturated with paraffine. The outer covering is made in solid colors or combination of two colors.

Double conductors for house wiring are of various kinds.
Two conductors twisted together, without any outside cover, form a convenient method of wiring for bells, telephones, etc. These conductors may be 18 B. \& S., with double braid Weatherproof or with Annunciator insulation.

Two-conductor Office wire may be two Office wires laid side by side and covered with a two-colored Office braid, or it may consist of two Annunciator wires so insulated.

Weatherproof cables consist of $18 \mathrm{~B} . \&$ S. G. Annunciator wires, twisted into a cable and covered with rubber tape and a braid of cotton saturated with Weatherproof insulation. They weigh about ten pounds per 1000 feet per conductor. For work inside building, in dry places, the rubber tape may be omitted, and the finishing braid made any color to correspond with the woodwork.

Lamp cord is furnished in silk or cotton insulation. Green and yellow is the standard color combination.

| Numbers, B. \& S. G. | Weights per 1000 feet. |  | Sizes of Lamp cord. |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Office wire. | $\begin{gathered} \text { Annunciator } \\ \text { wire. } \end{gathered}$ | Silk. | Cotton. |
| $\begin{aligned} & 14 \\ & 16 \\ & 18 \\ & 20 \end{aligned}$ | 17 12 9 7 | $\begin{aligned} & 15 \\ & 10 \\ & 7 \\ & 41 / 2 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1 / 4 \\ & 10 \\ & 10 \\ & 18 \\ & 18 \end{aligned}$ |  |

## POWER CABLES.

WE MANUFACTURE power and electric-light cables, with jute, paper or rubber insulation. The thickness and kind of insulation depend on the use for which the cable is intended. The table of diameters and weights is based on $\frac{3}{16}$ insulation on a side, and is approximately correct for any kind of insulation.

## Specifications for Underground Cable of 500000 C. M.

## 1. Copper Conductor.

The conductor shall consist of 47 wires, each 104 mils in diameter, and shall weigh not less than 1.525 pounds per foot. The copper used shall have a conductivity of not less than 98 per cent.

## 2. Insulation.

The insulation shall consist of paper not less than ${ }^{3}$. thick, and shall form a wall of uniform thickness around the conductor.

## 3. Sheath.

The insulated conductor shall be enclosed in a pipe composed of lead and tin. The amount of tin shall not be less than 2.9 per cent. The pipe shall be formed around the core, and shall be free from holes or other defects, and of uniform thickness and composition.
4. Insulation Resistance.

The insulation resistance shall be not less than 300 megohms per mile, at $60^{\circ} \mathrm{F}$.

## POWER CABLES.

| Numbers, B. \& S. G. | Circular mils. | Outside diameters. Inches. | Weights, 1000 feet. Pounds. |
| :---: | :---: | :---: | :---: |
| $\ldots$ | 1000000 | 118 | 6685 |
| ....... | 900.000 | $1{ }^{23}$ | 6228 |
| .... | 800000 | $12 \frac{1}{3}$ | 5773 |
| ........ | 750000 | 15/8 | 5543 |
| ........ | 700000 | $11{ }^{19}$ | 5315 |
| ........ | 650000 | $1{ }_{18}{ }^{\frac{1}{8}}$ | 5088 |
| ....... | 600000 | $11 \frac{7}{2}$ | 4857 |
| ........ | 550000 | 11/2 | 4630 |
| .... | 500000 | 17 | 4278 |
| ........ | 450000 | 18/8 | 3923 |
| ....... | 400000 | 113 | 3619 |
| ........ | 350000 | $1 \frac{5}{88}$ | 3416 |
| ........ | 300000 | 11/4 | 3060 |
| *...... | 250000 | $1{ }_{18}{ }^{3}$ | 2732 |
| 0000 | 211600 | 138 | 2533 |
| 000 | 168100 | $1{ }_{17}^{18}$ | 2300 |
| 00 | 133225 | 1 | 2021 |
| 0 | 105625 | $1{ }^{18}$ | 1772 |
| 1 | 83521 | 29 | 1633 |
| 2 | 66564 | 7/8 | 1482 |
| 3 | 52441 | ${ }^{35}$ | 1360 |
| 4 | 41616 | 8/4 | 1251 |
| 6 | 26244 | $\frac{1}{18}$ | 1046 |

## TELEPHONE CABLES.

## Lead-encased for underground or aerial use.

THE INSULATION of these cables is dry paper. We manufacture several styles of 19 B. \& S. G., 20 B. \& S. G., and 22 B. \& S. G., according to the use for which they are intended. The most common size is 19 B. \& S. G. We also supply terminals and hangers. To determine the size supporting strand to use with these cables, consult tables page 39.

## Specifications for Telephone Cables.

## 1. Conductors.

Each conductor shall be . 03589 inches in diameter, ( 19 B. \& S. G.,) and have a conductivity of 98 per cent. of that of pure soft copper.
2. Core.

The conductor shall be insulated, twisted in pairs, the length of the twist not to exceed three inches, and formed into a core arranged in reverse layers.

## 3. Sheath.

The core shall be enclosed in a pipe composed of lead and tin, the amount of the tin shall be not less than $2 \mathrm{\circ}$ 号 per cent. The pipe shall be formed around the core, and shall be free from holes or other defects, and of uniform thickness and composition.

## 4. Electrostatic Capactity.

The average electrostatic capacity shall not exceed .080 of a microfarad per mile, each wire being measured against all the rest and a sheath grounded; the electrostatic capacity of any wires so measured shall not exceed .085 of a microfarad per mile.

## 5. Insulation Resistance.

Each wire shall show an insulation of not less than 500 megohms per mile, at $60^{\circ} \mathrm{F}$., when laid, spliced and connected to terminal ready for use; each wire being measured against all the rest and sheath grounded.

## 6. Conductor Resistance.

Each conductor shall have a resistance of not more than 47 B. A. ohms, at $60^{\circ} \mathbf{F}$., for each mile of cable, after the cable is laid and connected to the terminals.

TELEPHONE CABLES.

| Number pairs. | Outside diameters. Inches. | Weights, 1000 feet. Pounds. |
| :---: | :---: | :---: |
| 1 | ${ }^{\frac{8}{18}}$ | 214 |
| 2 | 3/8 | 302 |
| 3 | $1 / 2$ | 515 |
| 4 | ${ }_{18} 9$ | 629 |
| 5 | 5/8 | 747 |
| 6 | $3{ }_{3}$ | 877 |
| 7 | 118 | 912 |
| 10 | 13 | 1214 |
| 12 | $1{ }^{18}$ | 1375 |
| 15 | 1 | 1566 |
| 18 | $1{ }_{16}^{16}$ | 1758 |
| 20 | 11/8 | 1940 |
| 25 | $1{ }_{18}^{88}$ | 2332 |
| 30 | $1{ }^{76}$ | 2748 |
| 35 | 11/2 | 2985 |
| 40 | $1{ }_{18}{ }^{9}$ | 3176 |
| 45 | 15/8 | 3365 |
| 50 | $13 / 4$ | 3678 |
| 55 | 11 눟 | 3867 |
| 60 | 17/8 | 4055 |
| 65 | 148 | 4241 |
| 70 | 2 | 4430 |
| 80 | 21/8 | 4804 |
| 90 | 21/4 | 5180 |
| 100 | 28/8 | 5505 |

## TELEGRAPH CABLES.

## Lead-encased for underground use.

THESE cables are made of either rubber, cotton or paper insulation. The sizes and weights are approximately correct for rubber and cotton insulation. Both sizes and weights are slightly reduced for paper insulation. In all cases the cables are lead-encased.

## Specifications for Telegraph Cables.

## 1. Conductors.

Each conductor shall be . 064 inches in diameter, ( 14 B. \& S. G., ) and have a conductivity of 98 per cent. of that of pure copper.

## 2. Core.

The conductors shall be insulated to $\frac{5}{32}$ with cotton, and formed into a core arranged in reverse layers. This core shall be dried and saturated with approved insulating compound.

## 3. Sheath.

The core shall be enclosed in a pipe composed of lead and tin. The amount of tin shall not be less than 2.9 per cent. The pipe shall be formed around the core, and shall be free from holes or other defects, and of uniform thickness and composition.

## 4. Insulation Resistance.

The wire shall show an insulation of not less than 300 megohms per mile, at $60^{\circ} \mathrm{F}$., when laid, spliced and connected to terminals ready for use, each wire being measured against all the rest and the sheath grounded.

## 5. Conductor Resistance.

Each conductor shall have a resistance of not more than 28 International ohms, at $60^{\circ} \mathrm{F}$., for each mile of cable, after the cable is laid and connected up to the terminals.

TELEGRAPH CABLES.

|  | 14 B. \& S. G. Insulated to $\frac{8}{32}$. |  | 16 B. \& S. G. Insulated to $\frac{5}{32}$. |  | 18 B. \& S. G. Insulated to $\frac{5}{32}$. |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |
| 1 | 8/8 | 308 | 8/8 | 299 | 8/8 | 291 |
| 2 | $\frac{7}{18}$ | 438 | $\frac{7}{10}$ | 421 | $\frac{13}{2}$ | 356 |
| 3 | 1/2 | 573 | 1/2 | 546 | $\frac{7}{16}$ | 421 |
| 4 | 5/8 | 810 | ${ }^{28}$ | 670 | 135 | 486 |
| 5 | $8 / 4$ | 972 | 5/8 | 793 | 1/2 | 551 |
| 6 | 178 | 1132 | 18 | 946 | $\frac{17}{3}$ | 616 |
| 7 | 7/8 | 1295 | $8 / 4$ | 965 | ${ }^{\circ} \mathrm{I}$ | 681 |
| 10 | $\frac{18}{68}$ | 1512 | $\frac{13}{13}$ | 1155 | 8/8 | 820 |
| 12 | $1 \frac{1}{18}$ | 1873 | 7/8 | 1327 | 3/4 | 978 |
| 15 | $1 \frac{3}{18}$ | 2263 | $\frac{18}{18}$ | 1518 | $\frac{1}{13}$ | 1148 |
| 18 | 11/4 | 2523 | $1{ }_{18}^{18}$ | 1880 | 7/8 | 1318 |
| 20 | $1{ }^{5} 8$ | 2756 | 11/8 | 2076 | $\frac{18}{18}$ | 1477 |
| 25 | $1{ }_{18}^{78}$ | 3250 | 18 | 2496 | 1 | 1690 |
| 30 | $1{ }^{18}$ | 3515 | 18/8 | 2768 | $1{ }_{18}^{18}$ | 1903 |
| 35 | $1 \frac{18}{18}$ | 3910 | $1{ }_{18}^{76}$ | 8040 | $1 \frac{18}{18}$ | 2116 |
| 40 | 13/4 | 4175 | 11/2 | 3312 | 11/4 | 2330 |
| 45 | 1119 | 4441 | $1{ }^{\text {I }}$ | 3533 | $1{ }_{3}{ }^{\text {g }}$ | 2471 |
| 50 | $1 \frac{18}{8}$ | 4835 | 15/8 | 3755 | $1{ }^{\frac{8}{88}}$ | 2628 |
| 55 | 2 | 5100 | 118 | 3978 | 18/8 | 2866 |
| 60 | $2 \frac{1}{16}$ | 5365 | 18/4 | 4200 | $17^{\prime} 6$ | 3104 |
| 65 | 21/8 | 5631 | 118 | 4422 | $1 \frac{18}{5}$ | 3245 |
| 70 | $2{ }^{\frac{3}{88}}$ | 5897 | 17/8 | 4644 | 11/2 | 3402 |
| 80 | $2 \frac{88}{88}$ | 6408 | 2 | 5087 | 15/8 | 3798 |
| 90 | $2 \frac{7}{18}$ | 6916 | $2 \frac{18}{18}$ | 5402 | $11 \frac{18}{8}$ | 4027 |
| 100 | $2 \frac{18}{18}$ | 7375 | $21 / 8$ | 5720 | $13 / 4$ | 4275 |

## AERIAL CABLES.

THESE cables are made from double-coated rubber wire, taped. After standing, the cable is doubletaped and covered with tarred jute, over which is placed a braid of heavy cotton saturated with Weatherproof compound. This outside covering protects the rubber from the action of the air and from mechanical injury. The separate wires are tested in water, and no wire is used which will not fully meet a water test. The result is a cable which will work under water as well as on a pole line, if there is no danger of mechanical injury. The ordinary size for telegraphic work is $14 \mathrm{~B} . \& \mathrm{~S}$. , insulated to $\frac{6}{52}$. A trace wire can be placed in each layer, if desired.

The size galvanized strand to support these cables may be found from the table page 39. Suppose the span is 130 feet and a 10 -conductor 14 B. \& S. G. Aerial cable is used, then from these tables it is seen a $\frac{1}{4}$-inch ordinary galvanized strand will support a cable weighing 423 pounds per 1000 feet, with a 130 -foot span.

## Specifications for 14 B. \& S. Aerial Cable.

## 1. Conductors.

Each conductor shall be .064 inches in diameter, ( 14 B. \& S. G.,) and have a conductivity of 98 per cent. of that of pure copper.

## 2. Core.

The conductors shall be insulated to $\frac{6}{32}$ with rubber and tape, and formed into a core arranged in reverse layers.

## 3. Protective Covering.

The core shall be covered with two wraps of friction tape and one wrap of tarred jute. Over this there shall be a braid saturated with Weatherproof compound.
4. Insulation Resistance.

Each wire shall show an insulation resistance of not less than 300 megohms per mile, at $60^{\circ} \mathrm{F}$., after being immersed in water 24 hours. This test shall be made on the core after all the conductors are laid up, but before the outside coverings are put on.

## 5. Conductor Resistance.

Each conductor shall have a resistance of not more than 28 International ohms, at $60^{\circ} \mathrm{F}$., for each mile of cable.

## AERIAL CABLES.

Rubber insulation.

|  | 14 B. \& S. G. Insulated to $\frac{6}{32}$. |  | 16 B. \& S. G. Insulated to ${ }^{\frac{5}{3}}$. |  | 18 B. \& S. G. Insulated to 吉. |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |
| 2 | $8 / 8$ | 102 | 8/8 | 92 | 8/8 | 82 |
| 3 | 1/2 | 149 | $\frac{7}{18}$ | 126 | $\frac{13}{3}$ | 104 |
| 4 | ${ }^{2} 8$ | 183 | 3/2 | 155 | ${ }_{18}$ | 127 |
| 5 | $\frac{1}{15}$ | 226 | 8/8 | 193 | 1/2 | 151 |
| 6 | $3 / 4$ | 260 | 113 | 222 | $\frac{9}{16}$ | 175 |
| 7 | $\frac{18}{88}$ | 297 | 3/4 | 251 | 5/8 | 200 |
| 10 | $1{ }^{1}$ | 401 | 7/8 | 335 | 12 | 256 |
| 12 | 1 | 465 | 18 | 393 | $8 / 4$ | 296 |
| 15 | $11 / 8$ | 563 | 1 | 468 | 13 | 355 |
| 18 | $1{ }_{18}{ }^{3}$ | 651 | $1{ }_{18}^{18}$ | 541 | 7/8 | 413 |
| 20 | 11/4 | 714 | 11/8 | 593 | ${ }^{\frac{29}{3}}$ | 452 |
| 25 | 13/8 | 863 | $1{ }^{3} 8$ | 708 | $\frac{18}{18}$ | 541 |
| 30 | $1{ }^{17}{ }^{7}$ | 1008 | 11/4 | 824 | 1 | 633 |
| 35 | $11 / 2$ | 1147 | 18 | 938 | $1{ }^{18}$ | 723 |
| 40 | $1{ }^{18}$ | 1268 | 18/8 | 1053 | 11/8 | 813 |
| 45 | 15/8 | 1431 | 11/2 | 1182 | $1{ }^{188}$ | 903 |
| 50 | $13 / 4$ | 1577 | 15/8 | 1311 | 11/4 | 994 |

## SUBMARINE CABLES.

|  | Outside diameters. | Armor wires. |  | Total weights. Pounds. |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Number of wires. | Numbers, <br> B. W. G. | 1000 feet. | Mile. |
| 1 | 7/8 | 12 | 8 | 1250 | 6600 |
| 2 | 1 | 15 | 8 | 1722 | 9092 |
| 3 | 11/8 | 14 | 6 | 2363 | 12477 |
| 4 | $1 \frac{18}{18}$ | 16 | 6 | 2794 | 14752 |
| 5 | $1 \frac{5}{16}$ | 16 | 6 | 2968 | 15671 |
| 6 | 11/2 | 16 | 4 | 3822 | 20180 |
| 7 | 11/2 | 16 | 4 | 3972 | 20972 |
| 10 | 17/8 | 18 | 3 | 5404 | 28533 |

The core consists of $7 \times 22 \mathrm{~B} . \& \mathrm{~S}$. tinned copper wires, insulated with rubber to $\frac{8}{32}$ of an inch, laid up with proper jute bedding.

We are prepared to furnish telegraph cables with gutta-percha insulation. This is the best insulation for submarine work, and its reliability and durability more than make up the difference in cost between it and any other insulation.

We are prepared to furnish submarine cables of any description for use in electric lighting and street railway work.

No list of these cables can be made, owing to the varying conditions to be met.

## THE COLUMBIA RAIL-BOND.

THE COLUMBIA BOND consists of three parts, two copper thimbles and the connecting copper rod. On each end of this copper rod is a truncated conehead with a fillet at the base. The inside of the thimble is tapered to fit the head on the bond, while the
 outside is slightly tapered in the opposite way.

In applying the bond, the cone-shaped heads are placed in the holes in the rail from one side and the thimbles are slipped over them from the other.
A portable hand-press is then applied, and the wedgeshaped head of the bond is forced into the thimble so that it is not possible to see the line separating the thimble and the head in a cross-section of the two.

The end of the head of the bond is expanded by a center-punch, held in position in the press.

When installed, owing to the pressure exerted between the head and the thimble, and also to the fact that they are of the same kind of metal, the two become one, both electrically and mechanically.

The contact of rail and bond is made by a wedge expanding the thimble against the hole in the rail, and, as the bond is wedged both ways, it cannot get loose.

For a 0000 B. \& S. G. or 000 B. \& S. G. bond, the holes in the rail should be $\frac{7}{8}$-inch, and for a 00 B . \& S. G. or a 0 B. \& S. G. bond, $\frac{5}{8}$-inch.

The total length of a bond is $3 \frac{1}{2}$ inches more than the distance from center to center of holes in rails. The total length of a bond should be 8 inches more than that of the splice plate.

## University of California

 SOUTHERN REGIONAL LIBRARY FACILITY 405 Hilgard Avenue, Los Angeles, CA 90024-1388 Return this material to the library from which it was borrowed.|  |  |
| :---: | :---: |
|  |  |


PLEASE DO NOT REMOVE THIS BOOK CARD 引
University Research Library


[^0]:    1 kilogram per square millimeter $=1423$ pounds per square inch.
    pound per square inch $=.000703$ kilograms per square millimeter.

[^1]:    1. In the following specification the term silver voltameter means the arrangement of apparatus by means of which an electric current is passed through a solution of nitrate of silver in water. The silver voltameter measures the total electrical quantity which has passed duriug the time of the experiment, and by noting this time the time average of the current, or, if the current has been kept constant, the current itself can be deduced.

    In employing the silver voltameter to measure currents of about one ampere, the following arrangements should be adopted:

    The kathode on which the silver is to be deposited should take the form of a platinum bowl not less than 10 centimeters in diameter and from 4 to 5 centimeters in depth.

    The anode should be a plate of pure silver, some 30 square centimeters in area and 2 or 3 milimeters in thickness.

    This is supported horizontally in the liquid near the top of the solution by a platinum wire passed through holes in the plate at opposite corners. To prevent the disintegrated silver which is formed on the anode from falling onto the kathode, the anode should be wrapped around with pure filter paper, secured at the back with sealing wax.

    The liquid should consist of a neutral solution of pure silver nitrate, containlng about 15 parts by welght of the nitrate to 85 parts of water.

    The resistance of the voltameter changes somewhat as the current

[^2]:    passes. To prevent these changes having too great an effect on the current, some resistance besides that of the voltameter should be inserted in the circuit. The total metallic resistance of the circuit should not be less than 10 ohms.
    2. A committee, consisting of Messrs. Helmholtz, Ayrton and Carhart, was appointed to prepare specifications for the Clark's cell. Their report has not yet been received.

[^3]:    RuLs.-To find strain in pounds on wire of given span and deflection, muitiply numbers in column answering to span and

